

Symbols

A	Cross-sectional area of a pile, Equation (4-9) Cross-sectional area of shear wall boundary members or diaphragm chords in. ² , Equations (8-2), (8-4), (8-5)	A_w	Area of shear reinforcement, Equation (7-12) Nominal area of the web, Equation (5-7) Area of link stiffener web, Equation (5-28), (5-31) Area of the web cross section, = $b_w d$, Chapter 6
A_b	Gross area of bolt or rivet, Equations (5-18), (5-22), (5-24) Sum of net mortared area of bed joints above and below the test unit, Equation (7-2)	A_x	Accidental torsion amplification factor, Equation (3-1)
A_c	Area of column, Equation (5-8)	B	Width of footing, Equations (4-6), (4-7), (4-8)
A_e	Effective net area of the horizontal leg, Equation (5-20)	B_1	Damping coefficient used to adjust one-second period spectral response for the effect of viscous damping, Equations (1-10), (1-11)
A_g	Gross area of the horizontal leg, Equation (5-19) Gross area of cast iron column, Equation (5-36) Gross area of column, in. ² , Equation (6-4)	B_{D1}	Numerical damping coefficient taken equal to the value of B_1 , as set forth in Table 1-6, at effective damping β equal to the value of β_D , Equation (9-2)
A_j	Effective cross-sectional area of a beam-column joint, in. ² , in a plane parallel to plane of reinforcement generating shear in the joint calculated as specified in Section 6.5.2.3.1, Equation (6-5)	B_{M1}	Numerical damping coefficient taken equal to the value of B_1 , as set forth in Table 1-6, at effective damping β equal to the value of β_M , Equation (9-4)
A_n	Area of net mortared/grouted section, Equations (7-1), (7-3), (7-5), (7-7), (7-9), (7-10), (7-11), (7-13)	B_S	Coefficient used to adjust short-period spectral response for the effect of viscous damping, Equations (1-8), (1-9), (1-11)
A_{ni}	Area of net mortared/grouted section of masonry infill, Equation (7-15)	C (or C_j)	Damping coefficient for viscoelastic device (or device j), Equations (9-22), (9-24), (9-29), (9-30), (9-35), (9-37)
A_s	Area of nonprestressed tension reinforcement, in. ² , Tables 6-18, 6-20 Area of reinforcement, Equation (7-13)	C_0	Modification factor to relate spectral displacement of an equivalent SDOF system to the roof displacement of the building MDOF system, Equation (3-15) Damping coefficient for fluid-viscous device, Equation (9-25)
$A's$	Area of compression reinforcement, in. ² , Tables 6-18, 6-20	C_1	Modification factor to relate expected maximum inelastic displacements to displacements calculated for linear elastic response, Equations (3-5), (3-6), (3-10), (3-15), (3-19)

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C_2	Modification factor to represent the effects of pinched hysteresis shape, stiffness degradation and strength deterioration on the maximum displacement response, Equations (3-5), (3-6), (3-10), (3-15), (3-19)	DCR	Demand-capacity ratio, computed in accordance with Equation (2-1) or required in Equation (2-2)
		$\overline{DCR}$	Average demand-capacity ratio for a story, computed in accordance with Equation (2-2)
C_3	Modification factor to represent increased displacements due to p- Δ effects, Equations (3-5), (3-6), (3-10), (3-15), (3-17), (3-19)	D_D	Design displacement, in. (mm) at the center of rigidity of the isolation system in the direction under consideration, Equations (9-2), (9-6), (9-8), (9-10), (9-14), (9-15), (9-18), (9-22)
C_b	Coefficient to account for effect of nonuniform moment given in AISC (1993) <i>LRFD Specifications</i> , Equation (5-9)	D'_D	Design Earthquake target displacement, in. (mm) at a control node located at the center of mass of the first floor above the isolation system in the direction under consideration, as prescribed by Equation (9-10)
CF_i	Stage combination factors for use with velocity-dependent energy dissipation devices as calculated by Equations (9-31) or (9-32)	D_M	Maximum displacement, in. (mm) at the center of rigidity of the isolation system in the direction under consideration, Equations (9-4), (9-7), (9-11), (9-16), (9-17), (9-19)
C_m	Effective mass factor from Table 3-1, Equations (3-10), (3-16)	D'_M	BSE-2 target displacement, in. (mm) at a control node located at the center of mass of the first floor above the isolation system in the direction under consideration, as prescribed by Equation (9-11)
C_t	Numerical value for adjustment of period T, Equation (3-7)	D_p	Relative seismic displacement that the component must be designed to accommodate, Equations (11-8), (11-9), (11-10), (11-11)
C_{vx}	Vertical distribution factor for the pseudo lateral load, Equations (3-11), (3-12)	D_r	Drift ratio for nonstructural components, Equation (11-7)
D	Generalized deformation, unitless Relative displacement between two ends of an energy dissipation unit, Equations (9-1), (9-20), (9-22)	D_{TD}	Total design displacement, in. (mm) of an element of the isolation system, including both translational displacement at the center of rigidity and the component of torsional displacement in the direction under consideration, as specified by Equation (9-6)
D^-	Maximum negative displacement of an energy dissipation unit, Equations (9-21), (9-23)		
D^+	Maximum positive displacement of an energy dissipation unit, Equations (9-21), (9-23)		
$\dot{D}$	Relative velocity between two ends of an energy dissipation unit, Equations (9-22), (9-25)		
D_{ave}	Average displacement of an energy dissipation unit, equal to $(D^+ + D^-)/2$, Equation (9-24)		
D_{clear}	Required clearance between a glass component and the frame, Equation (11-9)		

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D_{TM}	Total maximum displacement, in. (mm) of an element of the isolation system, including both translational displacement at the center of rigidity and the component of torsional displacement in the direction under consideration, as specified by Equation (9-7)	F_{cr}	Allowable axial buckling stress, see Equation (5-36)
E	Young's modulus of elasticity, Equations (4-9), (5-1), (5-2), (5-17), (8-2), (8-4), (8-5)	F_{EXX}	Classification strength of weld metal, Chapter 5
E_c	Modulus of elasticity of concrete, psi, Equation (6-6)	F_i	Inertia force at floor level i , Equation (9-27)
E_{fe}	Expected elastic modulus of frame material, ksi, Equation (7-14)		Lateral load applied at floor level i , Equation (3-13)
E_{Loop}	Energy dissipated, in kip-inches (kN-mm), in an isolator unit during a full cycle of reversible load over a test displacement range from Δ^+ to Δ^- , as measured by the area enclosed by the loop of the force-deflection curve, Equation (9-13)	F_{mi}	m -th mode horizontal inertia force at floor level i , Equation (9-34)
E_{me}	Expected elastic modulus of masonry in compression as determined per Section 7.3.2.4, Equation (7-14)	F_p	Horizontal seismic force for design of a structural or nonstructural component and its connection to the structure, Equations (2-3), (2-4), (2-5), (2-6), (2-7)
E_s	Modulus of elasticity of reinforcement, psi, Chapter 6		Component seismic design force applied horizontally at the center of gravity of the component or distributed according to the mass distribution of the component, Equations (11-1), (11-2), (11-3), (11-4)
E_{se}	Expected elastic modulus of reinforcing steel per Section 7.3.2.8	F_{pv}	Component seismic design force applied vertically at the center of gravity of the component or distributed according to the mass distribution of the component, Equations (11-2), (11-5), (11-6)
F	Force in an energy dissipation unit, Equations (9-1), (9-20), (9-22), (9-25)	F_{px}	Diaphragm lateral force at floor level x , Equation (3-13)
F^-	Negative force, in k, in an isolator or energy dissipation unit during a single cycle of prototype testing at a displacement amplitude of Δ^- , Equations (9-12), (9-21), (9-23), (9-38)	F_{te}	Expected tensile strength, Equations (5-20), (5-22), (5-24)
F^+	Positive force, in k, in an isolator or energy dissipation unit during a single cycle of prototype testing at a displacement amplitude of Δ^+ , Equations (9-12), (9-21), (9-23), (9-38)	F_v	Factor to adjust spectral acceleration at one second for site class, Equation (1-8)
F_a	Factor to adjust spectral acceleration in the short-period range for site class, Equation (1-7)		Design shear strength of bolts or rivets, Chapter 5
		F_{ve}	Unfactored nominal shear strength of bolts or rivets given in AISC(1993) <i>LRFD Specifications</i> , Equation (5-18)
		F_x	Lateral load applied at floor level x , Equation (3-11)
		F_y	Specified minimum yield stress for the type of steel being used, Equation (5-7)
		F_{yb}	F_y of a beam, Chapter 5
		F_{yc}	F_y of a column, Chapter 5

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F_{ye}	Expected yield strength, Equations (5-1) to (5-8), (5-19), (5-23), (5-25), (5-31), (5-34)	J	A coefficient used in linear procedures to estimate the actual forces delivered to force-controlled components by other (yielding) components, Equations (3-5), (3-19)
F_{yf}	F_y of a flange, Chapter 5	K	Length factor for brace; defined in AISC (1993) <i>LRFD Specifications</i> , Chapter 5
F_{yLB}	Lower-bound yield strength, Chapter 5	K'	Storage stiffness as prescribed by Equation (9-23)
G	Soil Shear modulus, Equation (4-6) Shear modulus of steel, Equations (5-28), (5-33) Modulus of rigidity of wood structural panels, psi, Equations (8-2), (8-4), (8-5)	K''	Loss stiffness as prescribed by Equation (9-24)
G_d	Shear stiffness of shear wall or diaphragm assembly, Equations (8-1), (8-3)	K_θ	Rotational stiffness of a partially restrained connection, Equations (5-15), (5-16), (5-17)
G_{me}	Shear modulus of masonry as determined per Section 7.3.2.7	K_b	Flexural stiffness, Equations (5-27), (5-29)
G_o	Initial or maximum shear modulus, Equations (4-4), (4-5)	K_{Dmax}	Maximum effective stiffness, in k/in., of the isolation system at the design displacement in the horizontal direction under consideration, as prescribed by Equation (9-14)
H	Thickness of a soil layer in feet, Chapter 11 Horizontal load on footing, Chapter 4	K_{Dmin}	Minimum effective stiffness, in k/in. (kN/mm), of the isolation system at the design displacement in the horizontal direction under consideration, as prescribed by Equation (9-15)
I	Moment of inertia, Equation (6-6)	K_e	Effective stiffness of the building in the direction under consideration, for use with the NSP, Equation (3-14)
I_b	Moment of inertia of a beam, Equations (5-1), (5-17)		Elastic stiffness of a link beam, Equations (5-27), (5-30)
I_c	Moment of inertia of a column, Equation (5-2)	K_i	Elastic stiffness of the building in the direction under consideration, for use with the NSP, Equation (3-14)
I_{col}	Moment of inertia of column section, Equation (7-14)	K_{Mmax}	Maximum effective stiffness, in k/in., of the isolation system at the maximum displacement in the horizontal direction under consideration, as prescribed by Equation (9-16)
I_f	Moment of inertia of most flexible frame member confining infill panel, Chapter 7	K_{Mmin}	Minimum effective stiffness, in k/in., of the isolation system at the maximum displacement in the horizontal direction under consideration, as prescribed by Equation (9-17)
I_g	Moment of inertia of gross concrete section about centroidal axis, neglecting reinforcement, Chapter 6		
I_p	Component performance factor; 1.0 shall be used for the Life Safety Nonstructural Performance Level and 1.5 shall be used for the Immediate Occupancy Nonstructural Performance Level, Equations (11-1), (11-3), (11-4), (11-5), (11-6)		

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K_s	Shear stiffness, Equations (5-27), (5-28)	M_{CEx}	Expected bending strength of a member about the x-axis, Equations (5-10), (5-11), (5-13), (6-1)
L	Length of footing in plan dimension, Equations (4-7), (4-8) Length of pile in vertical dimension, Equation (4-9) Length of member along which deformations are assumed to occur, Chapter 6 Length of wall or pier, Equations (7-4), (7-5) Diaphragm span, distance between shear walls or collectors, Equations (8-3), (8-4), (8-5)	M_{CEy}	Expected bending strength of a member about y-axis, Equations (5-10), (5-11), (5-13), (6-1)
L_b	Length or span of beam, Equations (5-6), (5-17) Distance between points braced against lateral displacement of the compression flange or between points braced to prevent twist of the cross-sections; given in AISC (1993) <i>LRFD Specifications</i> , Equation (5-9)	M_{CLx}	Lower-bound flexural strength of the member about the x-axis, Equation (5-12)
		M_{CLy}	Lower-bound flexural strength of the member about the y-axis, Equation (5-12)
		M_{gCS}	Moment acting on the slab column strip, Chapter 6
		M_n	Nominal moment strength at section, Chapter 6
		M_{nCS}	Nominal moment strength of the slab column strip, Chapter 6
L_{inf}	Length of infill panel, Equations (7-17), (7-19)	M_{OT}	Total overturning moment induced on the element by seismic forces applied at and above the level under consideration, Equations (3-5), (3-6)
L_p	The limiting unbraced length between points of lateral restraint for the full plastic moment capacity to be effective; given in AISC (1993) <i>LRFD Specifications</i> , Equations (5-6), (5-9)	M_{PCE}	Expected plastic moment capacity, Equation (5-6)
		M_{ST}	Stabilizing moment produced by dead loads acting on the element, Equations (3-5), (3-6)
L_r	The limiting unbraced length between points of lateral support beyond which elastic lateral torsional buckling of the beam is the failure mode; given in AISC (1993) <i>LRFD Specifications</i> , Equation (5-9)	M_{UD}	Design moment, Chapter 6
		M_{UDx}	Design bending moment about x axis for axial load P_{UF} , kip-in., Equation (6-1)
		M_{UDy}	Design bending moment about y axis for axial load P_{UF} , kip-in., Equation (6-1)
M	Design moment at a section, Equation (6-4) Moment on masonry section, Equation (7-11)	M_{UFx}	Bending moment in the member about the x-axis, calculated in accordance with Section 3.4.2.1.2, Equation (5-12)
M_c	Ultimate moment capacity of footing, Equation (4-8)	M_{UFy}	Bending moment in the member about the y-axis, calculated in accordance with Section 3.4.2.1.2, Equation (5-12)
M_{CE}	Expected flexural strength of a member or joint, Equation (5-3), (5-4), (5-6), (5-15), (5-16), (5-18), (5-22), (5-24), (5-25), (5-26), (5-32)	M_x	Bending moment in a member for the x-axis, Equations (5-10), (5-11), (5-13)

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M_y	Bending moment in a member for the y-axis, Equations (5-10), (5-11), (5-13) Yield moment strength at section, Equation (6-6)	P_i	Portion of the total weight of the structure including dead, permanent live, and 25% of transient live loads acting on the columns and bearing walls within story level i , Equation (3-2)
N	Number of piles in a pile group, Equation (4-9)	P_o	Nominal axial load strength at zero eccentricity, Chapter 6
$\bar{N}$	Average SPT blow count in soil within the upper 100 feet of soil, calculated in accordance with Equation (2-8)	P_R	Mean return period, Equation (1-2)
$(N_1)_{60}$	Standard Penetration Test blow count normalized for an effective stress of 1 ton per square foot and corrected to an equivalent hammer energy efficiency of 60%, Equation (4-5)	P_{UF}	Design axial force in a member, Equations (5-10), (5-11), (5-12)
N_b	Number of bolts or rivets, Equations (5-18), (5-22), (5-24)	P_{ye}	Expected yield axial strength of a member, Equations (5-2), (5-4)
N_u	Factored axial load normal to cross-section occurring simultaneously with V_u . To be taken as positive for compression, negative for tension, and to include effects of tension due to creep and shrinkage, Equation (6-4)	Q	Generalized force in a component, Figures 2-3, 2-5, 5-1, 6-1, 7-1, 8-1
P	Vertical load on footing, Equation (4-8) Axial force in a member, Equations (5-2), (5-4)	Q_{allow}	Allowable bearing load specified for the design of deep foundations for gravity loads (dead plus live loads) in the available design documents, Equation (4-2)
P_c	Lower bound of vertical compressive strength for wall or pier, Equations (7-7), (7-13)	Q_c	Expected bearing capacity of deep or shallow foundation, Equations (4-2), (4-3), (4-7)
P_{CE}	Expected axial strength of a member or joint, Equations (5-19), (5-20), (5-21), (5-26) Expected gravity compressive force, Equations (7-1), (7-4)	Q_{CE}	Expected strength of a component or element at the deformation level under consideration, Equations (2-1), (3-20), (5-3) to (5-8), (5-18), (5-22), (5-24), (5-25), (5-26), (5-30), (5-31), (5-32), (5-34), (5-35), (7-3), (7-4), (7-15)
P_{CL}	Lower-bound axial strength of column, Equations (5-10), (5-11), (5-12), (5-36) Lower bound axial compressive force due to gravity loads specified in Equation (3-4)	Q_{CEb}	Expected bending strength of the beam, Equation (5-14)
P_{EY}	Probability of exceedance in Y years, expressed as a decimal, Equation (1-2)	Q_{CL}	Lower-bound estimate of the strength of a component or element at the deformation level under consideration, Equations (3-21), (5-36), (6-5), (7-5) to (7-8), (7-13), (7-21)
PI	Plasticity Index for soil, determined as the difference in water content of soil at the liquid limit and plastic limit, Section 1.6.1.4.1	Q_{CLc}	Lower-bound strength of the connection, Equation (5-14)
		Q_D	Design action due to dead load, Equations (3-3), (3-4)
		Q_E	Design action due to design earthquake loads, Equations (3-18), (3-19)

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Q_G	Design action due to gravity loads, Equation (3-3), (3-4), (3-18), (3-19)	S_{XS}	Spectral response acceleration parameter at short periods for the selected Earthquake Hazard Level and damping, adjusted for site class, and determined in accordance with Section 1.6.1.4 or 1.6.2.1, Equation (1-4), (1-8), (1-9), (1-11), (1-13), (1-14), (1-15), (1-16), (4-11), (11-1), (11-3), (11-4), (11-5), (11-6)
Q_L	Design action due to live load, Equations (3-3), (3-4)	T	Fundamental period of the building in the direction under consideration, seconds, Equations (1-8), (1-10), (3-7), (3-8), (3-9), (3-10), (9-29)
Q_S	Design action due to snow load, Equations (3-3), (3-4)		Tensile load in column, Equation (5-13)
Q_{UD}	Deformation-controlled design action due to gravity and earthquake loads, Equations (2-1), (3-18), (3-20)	T_0	Period at which the constant acceleration region of the design response spectrum begins at a value = $0.2T_S$, Equations (1-8), (1-12)
Q_{UF}	Force-controlled design action due to gravity and earthquake loads, Equations (3-19), (3-21))	T_{CE}	Expected tensile strength of column computed in accordance with Equation (5-8)
Q_y	Yield strength of a component, Figures 2-3, 2-5	T_D	Effective period, in seconds, of the seismic-isolated structure at the design displacement in the direction under consideration, as prescribed by Equation (9-3)
Q'_y	Substitute yield strength, Figure 2-5	T_e	Effective fundamental period of the building in the direction under consideration, for use with the NSP, Equations (3-14), (3-15), (3-17)
R	Ratio of the elastic-strength demand to the yield-strength coefficient, Equations (3-15), (3-16), (3-17)		Effective fundamental period, in seconds, of the building structure above the isolation interface on a fixed base in the direction under consideration, Equations (9-10), (9-11)
R_{OT}	Response modification factor for overturning moment M_{OT} , Equation (3-6)	T_i	Elastic fundamental period of the building in the direction under consideration, for use with the NSP, Equation (3-14)
R_p	Component response modification factor from Table 11-2, Equation (11-3))	T_M	Effective period, in seconds, of the seismic-isolated structure at the maximum displacement in the direction under consideration, as prescribed by Equation (9-5)
S_1	Spectral response acceleration parameter at a one-second period, obtained from response acceleration maps, Equations (1-1), (1-3), (1-5)	T_m	m-th mode period of the rehabilitated building including the stiffness of the velocity-dependent devices, Equation (9-35)
S_a	Spectral response acceleration, g , Equations (1-8), (1-9), (1-10), (3-10), (3-15), (3-16)		
S_n	Distance between n th pile and axis of rotation of a pile group, Equation (4-10)		
S_S	Spectral response acceleration parameter at short periods, obtained from response acceleration maps, Equations (1-1), (1-3), (1-7)		
S_{X1}	Spectral response acceleration parameter at a one-second period for any earthquake hazard level and any damping, adjusted for site class, Equations (1-5), (1-10), (1-11), (1-13), (1-14), (1-15), (1-16)		

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T_S	Period at which the constant acceleration region of the design response spectrum transitions to the constant velocity region, Equations (1-8), (1-9), (1-10), (1-11), (1-12), (1-13), (3-10), (3-15)	V_i	The total calculated lateral shear force in the direction under consideration in an element or at story i due to earthquake response to the selected ground shaking level, as indicated by the selected linear analysis procedure, Equations (2-2), (3-2)
T_{ss}	Secant fundamental period of a rehabilitated building calculated using Equation (3-14) but replacing the effective stiffness (K_e) with the secant stiffness (K_s) at the target displacement, Equation (9-37)	V_{ine}	Expected shear strength of infill panel, Equation (7-15)
V	Pseudo lateral load, Equations (3-10), (3-11) Design shear force at section, Equation (6-4) Shear on masonry section, Equation (7-11)	V_{mL}	Lower bound shear strength provided by masonry, Equations (7-8), (7-11)
V^*	Modified equivalent base shear, Chapter 9	V_n	Nominal shear strength at section, Equation (6-5)
V_b	The total lateral seismic design force or shear on elements of the isolation system or elements below the isolation system, as prescribed by Equation (9-8)	V_o	Shear strength of slab at critical section, Chapter 6
V_{bjs}	Expected shear strength of wall or pier based on bed-joint sliding shear stress, see Equation (7-3)	V_{pz}	Panel zone shear, Chapter 5
V_c	Nominal shear strength provided by concrete, Equation (6-4)	V_r	Expected shear strength of wall or pier based on rocking shear, Equation (7-4)
V_{CE}	Expected shear strength of a member, Equations (5-11), (5-31), (5-32), (5-34)	V_s	Nominal shear strength provided by shear reinforcement, Chapter 6 The total lateral seismic design force or shear on elements above the isolation system, as prescribed by Section 9.2.4.4.2, Equation (9-9)
V_{CL}	Lower bound shear strength, Equations (7-8), (7-9), (7-10)	V_{sL}	Lower bound shear strength provided by shear reinforcement, Equations (7-8), (7-12)
V_{dt}	Lower bound shear strength based on diagonal tension stress for wall or pier, Chapter 7	V_t	Base shear in the building at the target displacement, Chapter 3
V_{fre}	Expected story shear strength of the bare steel frame taken as the shear capacity of the column, Chapter 7	V_{tc}	Lower bound shear strength based on toe compressive stress for wall or pier, Chapter 7
V_g	Shear acting on slab critical section due to gravity loads, Chapter 6	V_{test}	Test load at first movement of a masonry unit, Equation (7-2)
		V_u	Factored shear force at section, Chapter 6
		V_y	Yield strength of the building in the direction under consideration, for use with the NSP, Equation (3-16)
		V_{ya}	Nominal shear strength of a member modified by the axial load magnitude, Chapter 5

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W	Weight of a component, calculated as specified in this standard, Chapter 2. Effective seismic weight of a building including total dead load and applicable portions of other gravity loads listed in Section 3.3.1.3.1, Equations (3-10), (3-16) The total seismic dead load in kips (kN). For design of the isolation system, W is the total seismic dead-load weight of the structure above the isolation interface, Equations (9-3), (9-5)	a	Parameter used to measure deformation capacity in component load-deformation curves, Figures 2-3, 5-1, 6-1 Clear width of wall between columns, Equations (5-33), (5-34) Equivalent width of infill strut, Equations (7-14), (7-16), (7-17), (7-18), (7-19)
W_D	Energy dissipated in a building or element thereof or energy dissipation device during a full cycle of displacement, Equations (9-24), (9-39)	a'	Parameter used to measure deformation capacity in component load-deformation curve, Figure 2-5
W_j	Work done by an energy dissipating device, j , in one complete cycle corresponding to floor displacement, Equations (9-26), (9-28), (9-29), (9-36), (9-37)	a_p	Component amplification factor from Table 11-2, Equation (11-3)
W_k	Maximum strain energy in a frame as calculated by Equation (9-27)	b	Parameter used to measure deformation capacity in component load-deformation curves, Figures 2-3, 5-1, 6-1 Shear wall length or width, Equations (8-1), (8-2) Diaphragm width, Equations (8-4), (8-5) The shortest plan dimension of the rehabilitated building, in ft. (mm), measured perpendicular to d , Equations (9-6), (9-7)
W_{mj}	Work done by device j in one complete cycle corresponding to modal floor displacements δ_{mi} Equation (9-33)	ba	Connection dimension, Equations (5-22), (5-23)
W_{mk}	Maximum strain energy in the frame in the m -th mode determined using Equation (9-34)	b_{bf}	Beam flange width in Equations for Beam-Column Connections in Sections 5.5.2.4.2 and 5.5.2.4.3
W_p	Component operating weight, Equations (11-1), (11-3), (11-4), (11-5), (11-6)	b_{cf}	Column flange width in Equations for Beam-Column Connections in Sections 5.5.2.4.2 and 5.5.2.4.3
X	Height of upper support attachment at level x as measured from grade, see Equation (11-7)	b_f	Flange width, Tables 5-5, 5-6, 5-7
Y	Time period in years corresponding to a mean return period and probability of exceedance, Equation (1-2) Height of lower support attachment at level y as measured from grade, see Equation (11-7)	b_p	Width of rectangular glass, Equation (11-9)
Z	Plastic section modulus, Equations (5-1), (5-2), (5-3), (5-4), (5-6)	b_t	Connection dimension, Equations (5-24), (5-25)
Z'	Adjusted resistance for mechanical fastener, Chapter 8	b_w	Web width, in., Equation (6-4)
		c	Parameter used to measure residual strength, Figures 2-3, 5-1, 6-1, 7-1, 8-1

Symbols

c_1	Size of rectangular or equivalent rectangular column, capital, or bracket measured in the direction of the span for which moments are being determined, in, Section 6.5.4.3 Clearance (gap) between vertical glass edges and the frame, Equation (11-9)	e	Length of EBF link beam, Equations (5-28), (5-29), (5-30), (5-32) Parameter used to measure deformation capacity, Figures 2-3, 5-1, 6-1, 7-1, 8-1 Actual eccentricity, ft. (mm), measured in plan between the center of mass of the structure above the isolation interface and the center of rigidity of the isolation system, plus accidental eccentricity, ft. (mm), taken as 5% of the maximum building dimension perpendicular to the direction of force under consideration, Equations (9-6), (9-7)
c_2	Clearance (gap) between horizontal glass edges and the frame, Equation (11-9)	e_n	Nail deformation at yield load per nail for wood structural panel sheathing, Equations (8-2), (8-4), (8-5)
d	Depth of soil sample for calculation of effective vertical stress, Equation (4-5) Parameter used to measure deformation capacity, Figures 2-3, 5-1, 6-1, 7-1, 8-1 Distance from extreme compression fiber to centroid of tension reinforcement, in., Equation (6-4) The longest plan dimension of the rehabilitated building, in ft. (mm), Equations (9-6), (9-7)	f_1	Fundamental frequency of the building, Equation (9-24)
d_a	Elongation of anchorage at end of wall determined by anchorage details and load magnitude, Equation (8-1) Deflection at yield of tie-down anchorage or deflection at load level to anchorage at end of wall determined by anchorage details and dead load, in., Equation (8-2)	f_a	Axial compressive stress due to gravity loads specified in Equations (3-3), (7-5), (7-6)
d_b	Overall beam depth, Equations (5-7), (5-8), (5-21), (5-22), (5-23), (5-24), (5-25), (5-26), (5-29) Nominal diameter of bar, in., Equation (6-3)	f_{ae}	Expected vertical compressive stress, Chapter 7
d_{bg}	Depth of the bolt group, Table 5-5	f_c	Compressive strength of concrete, psi, Equations (6-4), (6-5)
d_c	Column depth, Equation (5-5)	f'_{dt}	Lower bound masonry diagonal tension strength, Equation (7-5)
d_i	Depth, in feet, of a layer of soils having similar properties, and located within 100 feet of the surface, Equations (1-6), (1-7)	f'_m	Lower bound masonry compressive strength, Equations (7-6), (7-7), (7-9), (7-10), (7-11), (7-13), (7-21)
d_v	Length of component in the direction of shear force, Equations (7-11), (7-12)	f_{me}	Expected compressive strength of masonry as determined in Section 7.3.2.3
d_w	Depth to ground-water level, Equation (4-5)	f_{pc}	Average compressive stress in concrete due to effective prestress force only (after allowance for all prestress losses), Chapter 6
d_z	Overall panel zone depth between continuity plates, Chapter 5	f_s	Stress in reinforcement, psi, Equations (6-2), (6-3)
		f'_t	Lower bound masonry tensile strength, Chapter 7
		f_{te}	Expected masonry flexural tensile strength as determined in Section 7.3.2.5

Symbols

f_{vie}	Expected shear strength of masonry infill, Equation (7-15)	h_n	Height to roof level, ft, Equation (3-7)
f_y	Yield strength of tension reinforcement, Equations (6-2), (6-3) Lower bound of yield strength of reinforcing steel, Equations (7-12), (7-13)	h_p	Height of rectangular glass, Equation (11-9)
f_{ye}	Expected yield strength of reinforcing steel as determined in Section 7.3.2.8	h_x	Height from base to floor level x , ft, Equations (3-12), (9-9)
g	Acceleration of gravity (386.1 in./sec. ² , or 9,807 mm/sec ² for SI units), Equations (3-15), (9-2), (9-3), (9-4), (9-5), (9-30)	k	Exponent used for determining the vertical distribution of lateral forces, Equation (3-12) Coefficient used for calculation of column shear strength, Chapter 6
h	Average story height above and below a beam-column joint, Equation (5-17) Clear height of wall between beams, Equations (5-33), (5-35) Distance from inside of compression flange to inside of tension flange, Equation (5-7) Height of member along which deformations are measured, Chapter 6 Overall thickness of member, in, Equation (6-4) Height of a column, pilaster, or wall, Chapter 7 Shear wall height, Equations (8-1), (8-2) Average roof elevation of structure, relative to grade elevation, Equation (11-3)	k_1	Distance from the center of the split tee stem to the edge of the split tee flange fillet, Equation (5-25)
		k_{eff}	Effective stiffness of an isolator unit, as prescribed by Equation (9-12), or an energy dissipation unit, as prescribed by Equations (9-23) or (9-38)
		k_h	Horizontal seismic coefficient in soil acting on retaining wall, Equation (4-11)
		k_{sr}	Winkler spring stiffness in overturning (rotation) for pile group, expressed as moment/unit rotation, Equation (4-10)
		k_{sv}	Winkler spring stiffness in vertical direction, expressed as force/unit displacement/unit area, Equation (4-6) Pile group axial spring stiffness expressed as force/unit displacement, Equation (4-9)
h_c	Assumed web depth for stability, Chapter 5 Gross cross-sectional dimension of column core measured in the direction of joint shear, in, Chapter 6	k_v	Shear buckling coefficient, Chapter 5
		k_{vn}	Axial stiffness of n th pile in a pile group, Equation (4-10)
h_{col}	Height of column between beam centerlines, Equation (7-14)	l_b	Length of beam, Equation (5-1) Provided length of straight development, lap splice, or standard hook, in., Equation (6-2)
h_{eff}	Effective height of wall or pier components under consideration, Equations (7-4), (7-5), (7-6)	l_{beff}	Assumed distance to infill strut reaction point for beams, Equation (7-18)
h_i	Height from the base of a building to floor level i , Equations (3-12), (9-9) Height of story i between two floors at common points of reference, Equation (3-2)	l_c	Length of column, Equations (5-2), (5-36)
		l_{ceff}	Assumed distance to infill strut reaction point for columns, Equation (7-16)
h_{inf}	Height of infill panel, Equations (7-14), (7-17), (7-19), (7-20), (7-21)		

Symbols

l_d	Required length of development for a straight bar, in., Equation (6-2)	r_{inf}	Diagonal length of infill panel, Equation (7-14)
l_e	Length of embedment of reinforcement, in., Equation (6-3)	s	Spacing of shear reinforcement, Equation (7-12)
l_p	Length of plastic hinge used for calculation of inelastic deformation capacity, in., Equation (6-6)	s_i	Minimum separation distance between adjacent buildings at level i , Equation (2-8)
l_w	Length of entire wall or a segment of wall considered in the direction of shear force, in., Chapter 6	s_u	Undrained shear strength of soil, pounds/ft. ² , Chapter 1
m	Modification factor used in the acceptance criteria of deformation-controlled components or elements, indicating the available ductility of a component action, Equations (3-20), (5-9)	$\overline{s_u}$	Average value of the undrained soil shear strength in the upper 100 feet of soil, calculated in accordance with Equation (1-6), pounds/ft. ²
m_e	Effective m -factor, Equation (5-9)	t	Effective thickness of wood structural panel or plywood for shear, in., Equations (8-2), (8-4), (8-5)
m_t	Value of m -factor for the column in tension, Equation (5-13)	t_a	Thickness of angle, Equations (5-21), (5-23)
m_x	Value of m for bending about x-axis of a member, Equations (5-10), (5-11), (5-13), (6-1)	t_{bf}	Thickness of beam flange, Chapter 5
m_y	Value of m for bending about y-axis of a member, Equations (5-10), (5-11), (5-13), (6-1)	t_{bw}	Thickness of beam web, Chapter 5
n	Total number of stories in a vertical seismic framing, Equations (3-12), (3-13)	t_{cf}	Thickness of column flange, Chapter 5
p_{D+L}	Expected gravity stress at test location, Equation (7-2)	t_{cw}	Thickness of column web, Chapter 5
q	Vertical bearing pressure, Equation (4-8)	t_f	Thickness of flange, Equations (5-25), (5-29)
q_{allow}	Allowable bearing pressure specified in the available design documents for the design of shallow foundations for gravity loads (dead plus live loads), Equation (4-1)	t_{inf}	Thickness of infill panel, Equations (7-14), (7-20), (7-21)
q_c	Expected bearing capacity of shallow foundation expressed in load per unit area, Equations (4-1), (4-3), (4-7), (4-8)	t_p	Thickness of panel zone including doubler plates, Equation (5-5) Thickness of flange plate, Equation (5-26)
q_{in}	Expected transverse strength of an infill panel, Equation (7-21)	t_s	Thickness of split tee stem, Equations (5-24), (5-25)
r	Governing radius of gyration, Equation (5-36)	t_w	Thickness of web, Equations (5-7), (5-29) Thickness of plate wall, Equation (5-33) Thickness of wall web, in., Chapter 6
		t_z	Thickness of panel zone (doubler plates not necessarily included), Chapter 5
		v	Maximum shear in the direction under consideration, Equation (8-5)

Symbols

v_{me}	Expected masonry shear strength, Equation (7-1) Expected masonry bed-joint sliding shear strength, Equation (7-3)	Δ^-	Negative displacement amplitude, in. (mm), of an isolator or energy dissipation unit during a cycle of prototype testing, Equations (9-12), (9-13), (9-38)
v_{te}	Average bed-joint shear strength, Equation (7-1)	Δ^+	Positive displacement amplitude, in. (mm), of an isolator or energy dissipation unit during a cycle of prototype testing, Equations (9-12), (9-13), (9-38)
v_{to}	Bed-joint shear stress from single test, Equation (7-2)		
v_y	Shear at yield in the direction under consideration in lb./ft., Equations (8-1), (8-2), (8-3), (8-4), (8-5)	Δ_{ave}	Average displacement of an energy dissipation unit during a cycle of prototype testing, equal to $(\Delta^+ + \Delta^-)/2$, Equation (9-39)
w	Water content of soil, calculated as the ratio of the weight of water in a unit volume of soil to the weight of soil in the unit volume, expressed as a percentage, Section 1.6.1.4.1 Length of connection member, see Equations (5-23), (5-25)	Δ_d	Diaphragm deformation, Equations (3-8), (3-9)
		Δ_{eff}	Differentiated displacement between the top and bottom of the wall or pier components under consideration over a height, h_{eff} , Figure 7-1
w_i	Portion of the effective seismic weight corresponding to floor level i , Equations (3-12), (3-13), (9-9)	$\Delta_{fallout}$	Relative seismic displacement (drift) causing glass fallout from the curtain wall, storefront, or partition, as determined in accordance with an approved engineering analysis method, Equations (11-10), (11-11)
w_x	Portion of the effective seismic weight corresponding to floor level x , Equations (3-12), (3-13), (9-9)		
w_z	Width of panel zone between column flanges, Chapter 5	Δ_i	Inter-story displacement (drift) of story i divided by the story height, Chapter 5
x	Elevation in structure of component relative to grade elevation, Equation (11-3)	Δ_{i1}	Estimated lateral deflection of building 1 relative to the ground at level i , Equation (2-8)
y	The distance, in ft. (mm), between the center of rigidity of the isolation system rigidity and the element of interest, measured perpendicular to the direction of seismic loading under consideration, Equations (9-6), (9-7)	Δ_{i2}	Estimated lateral deflection of building 2 relative to the ground at level i , Equation (2-8)
		Δ_{inf}	Deflection of infill panel at mid-length when subjected to transverse loads, Equation (7-20)
Δ	Generalized deformation, Figures 2-3, 2-5, 5-1, 6-1, 8-1 Total elastic and plastic displacement, Chapter 5 Calculated deflection of diaphragm, wall, or bracing element, in.	Δ_p	Additional earth pressure on retaining wall due to earthquake shaking, Equation (4-11)
		Δ_w	Average in-plane wall displacement, Equation (3-8)

Symbols

Δ_y	Generalized yield deformation, unitless, Figure 5-1 Calculated deflection of diaphragm, shear wall, or bracing element at yield, see Equations (8-1), (8-2), (8-3), (8-4), (8-5)	$\Sigma F^-_M _{max}$	Sum, for all isolator units, of the maximum absolute value of force, in kips (kN), at a negative displacement equal to D_M , Equation (9-16)
$\Sigma(\Delta_c X)$	Sum of individual chord-splice slip values on both sides of the diaphragm, each multiplied by its distance to the nearest support, Equations (8-4), (8-5)	$\Sigma F^-_M _{min}$	Sum, for all isolator units, of the minimum absolute value of force, in kips (kN), at a negative displacement equal to D_M , Equation (9-17)
ΣE_D	Total energy dissipated, in in-kips, in the isolation system during a full cycle of response at the design displacement, D_D , Equation (9-18)	α	Ratio of post-yield stiffness to effective stiffness, Equation (3-17) Factor equal to 0.5 for fixed-free cantilevered shear wall, or 1.0 for fixed-fixed pier, Equation (7-4)
ΣE_M	Total energy dissipated, in in-kips, in the isolation system during a full cycle of response at the maximum displacement, D_M , Equation (9-19)		Velocity exponent for a fluid viscous device in Equation (9-25)
$\Sigma F^+_D _{max}$	Sum, for all isolator units, of the maximum absolute value of force, in kips (kN), at a positive displacement equal to D_D , Equation (9-14)	β	Modal damping ratio, Table 1-6 Factor to adjust fundamental period of the building, Equation (3-7) Ratio of expected frame strength, v_{fre} , to expected infill strength, v_{ine} , Chapter 7 Damping inherent in the building frame (typically equal to 0.05), Equations (9-26), (9-28), (9-30)
$\Sigma F^+_D _{min}$	Sum, for all isolator units, of the minimum absolute value of force, in kips (kN), at a positive displacement equal to D_D , Equation (9-15)	β_b	Equivalent viscous damping of a bilinear system, Chapter 9
$\Sigma F^+_M _{max}$	Sum, for all isolator units, of the maximum absolute value of force, in kips (kN), at a positive displacement equal to D_M , Equation (9-16)	β_D	Effective damping of the isolation system at the design displacement, as prescribed by Equation (9-18))
$\Sigma F^+_M _{min}$	Sum, for all isolator units, of the minimum absolute value of force, in kips (kN), at a positive displacement equal to D_M , Equation (9-17)	β_{eff}	Effective damping of isolator unit, as prescribed by Equation (9-13), or an energy dissipation unit, as prescribed by Equation (9-39); also used for the effective damping of the building, as prescribed by Equations (9-26), (9-28), (9-30), (9-31), (9-32), (9-36)
$\Sigma F^-_D _{max}$	Sum, for all isolator units, of the maximum absolute value of force, in kips (kN), at a negative displacement equal to D_D , Equation (9-14)	β_{eff-m}	Effective damping in m -th mode prescribed by Equation (9-33)
$\Sigma F^-_D _{min}$	Sum, for all isolator units, of the minimum absolute value of force, in kips (kN), at a negative displacement equal to D_D , Equation (9-15)	β_M	Effective damping of the isolation system at the maximum displacement, as prescribed by Equation (9-19))
		β_m	m -th mode damping in the building frame, Equation (9-33)

Symbols

γ	Unit weight, weight/unit volume (pounds/ft ³ or N/m ³), Equation (4-4) Coefficient for calculation of joint shear strength, Equation (6-5)	θ	Generalized deformation, radians, Figures 5-1, 6-1 Angle between infill diagonal and horizontal axis, $\tan\theta = h_{inf}/L_{inf}$, radians, see Equation (7-14)
γ_f	Fraction of unbalanced moment transferred by flexure at slab-column connections, Chapter 6	θ_b	Angle between lower edge of compressive strut and beam, radians, Equations (7-18), (7-19)
γ_t	Total unit weight of soil, Equations (4-5), (4-11)	θ_c	Angle between lower edge of compressive strut and column, radians, Equations (7-16), (7-17)
γ_w	Unit weight of water, Equation (4-5)	θ_i	Stability coefficient indicative of the stability of a structure under gravity loads and earthquake-induced deflection, Equation (3-2) Inter-story drift ratio, radians, Chapter 5
δ_i	Lateral drift in story i , in the direction under consideration, at its center of rigidity, using the same units as for measuring h_i , Equation (3-2) Displacement at floor i , Equations (9-26), (9-27)	θ_j	Angle of inclination of energy dissipation device, Equation (9-30)
δ_{mi}	m -th mode horizontal displacement at floor i , Equation (9-34)	θ_y	Generalized yield deformation, radians, Figure 5-1 Yield rotation, radians, Equations (5-1), (5-2), (5-30), (5-35), (6-6)
δ_{mrj}	m -th relative displacement between the ends of device j along its axis, Equation (9-35)	κ	A knowledge factor used to reduce component strength based on the level of knowledge obtained for individual components during data collection, Equations (3-20), (3-21), (6-1)
δ_{rj}	Relative displacement between the ends of energy dissipating device j along the axis of the device, Equations (9-29), (9-37)	λ	Correction factor related to unit weight of concrete, Equation (6-5)
δ_t	Target displacement, Figure 3-1	λ_1	Coefficient used to determine equivalent width of infill strut, Equation (7-14)
δ_{xA}	Deflection at level x of Building A, determined by an elastic analysis as defined in Chapter 3, Equations (11-7), (11-8)	λ_2	Infill slenderness factor, Equation (7-21)
δ_{xB}	Deflection at level x of Building B, determined by an elastic analysis as defined in Chapter 3, Equation (11-8)	λ_p	Limiting slenderness parameter for compact element, Chapter 5
δ_{yA}	Deflection at level y of Building A, determined by an elastic analysis as defined in Chapter 3, Equation (11-7)	λ_r	Limiting slenderness parameter for noncompact element, Chapter 5
η	Displacement multiplier, greater than 1.0, to account for the effects of torsion, Equation (3-1)	μ	Coefficient of shear friction, Chapter 6
		ν	Poisson's ratio of soil, Equation (4-4)

Symbols

v_s	Shear wave velocity in soil, in feet/sec., Section 1.6.1.4.1 Shear wave velocity at low strains, Equation (4-4)
$\overline{v_s}$	Average value of the soil shear wave velocity in the upper 100 feet of soil, calculated in accordance with Equation (1-6), feet/sec.
ρ	Ratio of non-prestressed tension reinforce- ment, Chapter 6
ρ_{bal}	Reinforcement ratio producing balanced strain conditions, Chapter 6
ρ_g	Ratio of area of total wall or pier vertical plus horizontal reinforcement to area of wall or pier cross-section, Chapter 7
ρ_{lp}	Yield deformation of a link beam, Chapter 5
ρ_n	Ratio of distributed shear reinforcement in a plane perpendicular to the direction of the applied shear, Chapter 6
ρ'	Ratio of non-prestressed compression reinforcement, Chapter 6
ρ''	Reinforcement ratio for transverse joint reinforcement, Chapter 6
σ	Standard deviation of the variation of the material strengths, Chapter 2
σ'_o	Effective vertical stress, Equation (4-5)
ϕ	Strength reduction factor
ϕ_i	Modal displacement of floor i , see Equation (9-30)
ϕ_{rj}	Relative modal displacement in horizontal direction of energy dissipation device j , Equation (9-30)
χ	A factor to calculate horizontal seismic force, F_p , Equations (2-6), (2-7)
ω_1	Fundamental angular frequency equal to $2\pi f_1$, Equation (9-24)