

- ## Seismic Hazard Analysis
- Deterministic procedures
 - Probabilistic procedures
 - USGS hazard maps
 - 2003 *NEHRP Provisions* design maps
 - Site amplification
 - *NEHRP Provisions* response spectrum
 - UBC response spectrum
- FEMA Instructional Material Complementing FEMA 451, Design Examples Seismic Hazard Analysis 5a - 2

Hazard vs Risk

Seismic hazard analysis describes the potential for dangerous, earthquake-related natural phenomena such as ground shaking, fault rupture, or soil liquefaction.

Seismic risk analysis assesses the probability of occurrence of losses (human, social, economic) associated with the seismic hazards.

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Approaches to Seismic Hazard Analysis

Deterministic
 "The earthquake hazard for the site is a peak ground acceleration of 0.35g resulting from an earthquake of magnitude 6.0 on the Balcones Fault at a distance of 12 miles from the site."

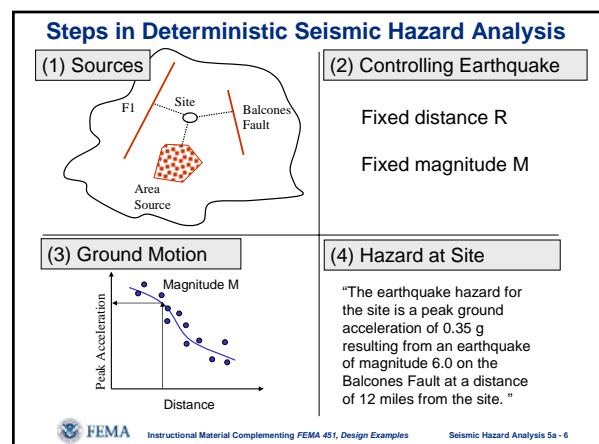
Probabilistic
 "The earthquake hazard for the site is a peak ground acceleration of 0.28g with a 2 percent probability of being exceeded in a 50-year period."

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Probabilistic Seismic Hazard Analysis

First addressed in 1968 by C. Allin Cornell in "Engineering Seismic Risk Analysis," and article in the *Bulletin of the Seismological Society* (Vol. 58, No. 5, October).

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Source Types

The diagram shows a central 'Site' marked with a dot. Two red lines labeled 'Fault' extend from the site. A red hatched area labeled 'Area Source' is located near the site. A larger red hatched area labeled 'Seismotectonic province' encompasses the site and the area source. A legend on the right lists:

- Fault
- Localizing structure
- Seismotectonic province

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Source Types

Localizing structure: An identifiable geological structure that is assumed to generate or “localize” earthquakes. This is generally a concentration of known or unknown active faults.

Seismotectonic province: A region where there is a known seismic hazard but where there are no identifiable active faults or localizing structures.

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Maximum Earthquake

Maximum possible earthquake: An upper bound to size (however unlikely) determined by earthquake processes (e.g., maximum seismic moment).

Maximum credible earthquake: The maximum reasonable earthquake size based on earthquake processes (but does not imply likely occurrence).

Maximum historic earthquake: The maximum historic or instrumented earthquake that is often a lower bound on maximum possible or maximum credible earthquake.

Maximum considered earthquake: Described later.

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Ground Motion Attenuation

The graph plots 'Ground Motion Parameter' on the y-axis against 'Distance' on the x-axis. A series of blue dots representing data points are connected by a downward-sloping curve. The curve is labeled 'Magnitude M'. To the right of the graph, the following reasons are listed:

- Geometric spreading
- Absorption (damping)

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Attenuation with Distance

The diagram shows a cross-section of the Earth's crust with a blue circular 'Area Source' at the bottom. A dashed line represents the path of seismic waves from the source to two recording stations. Above each station, a blue waveform shows the recorded seismic signal. The amplitude of the waveforms decreases as the distance from the source increases, illustrating attenuation.

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Comparison of Attenuation for Four Earthquakes

The map shows the United States with four shaded circular regions representing the attenuation zones for major earthquakes:

- 1906 SAN FRANCISCO
- 1971 SAN FERNANDO
- 1811 NEW MADRID
- 1888 CHARLESTON

 The zones are centered on the respective earthquake locations. A scale bar at the bottom right indicates 0, 250, and 500 miles.

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Ground Motion Attenuation Steps to Obtain Empirical Relationship

1. Obtain catalog of appropriate ground motion records
2. Correct for aftershocks, foreshocks
3. Correct for consistent magnitude measure
4. Fit data to empirical relationship of type:

$$\ln \hat{Y} = \ln b_1 + f_1(M) + \ln f_2(R) + \ln f_3(M, R) + \ln f_4(P_i) + \ln \varepsilon$$



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Ground Motion Attenuation Basic Empirical Relationships

$$\ln \hat{Y} = \ln b_1 + f_1(M) + \ln f_2(R) + \ln f_3(M, R) + \ln f_4(P_i) + \ln \varepsilon$$

\hat{Y} Ground motion parameter (e.g. PGA)

b_1 Scaling factor

$f_1(M)$ Function of magnitude

$f_2(R)$ Function of distance

$f_3(M, R)$ Function of magnitude and distance

$f_4(P_i)$ Other variables

ε Error term



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Ground Motion Attenuation Relationships for Different Conditions

- Central and eastern United States
- Subduction zone earthquakes
- Shallow crustal earthquakes
- Near-source attenuation
- Extensional tectonic regions
- Many others

May be developed for any desired quantity (PGA, PGV, spectral response).



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Ground Motion Attenuation Relationships

Seismological Research Letters
Volume 68, Number 1
January/February, 1997



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Earthquake Catalog for Shallow Crustal Earthquakes (Sadigh, Chang, Egan, Makdisi, and Youngs)

TABLE 1
List of Earthquakes Used to Develop Attenuation Relationships

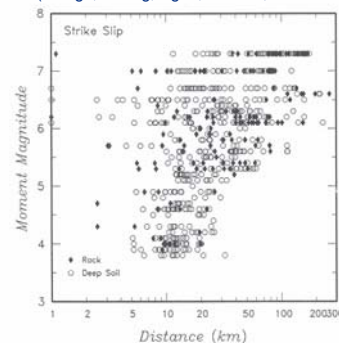
Earthquake	Date	M	Fault Type ¹	Distance Range (km)	No. of Records ²	
					R	DS
Kern County, CA	1952/07/21	7.4	RV	120.5-224.0	0	3
Port Hueme, CA	1957/09/18	4.7	RV	14.1-14.1	0	1
Daly City, CA	1957/03/22	5.3	RV	9.5-9.5	1	0
Parkfield, CA	1966/06/27	6.1	SS	0.1-230.0	1	6
Borrego Mtn., CA	1968/04/09	6.6	SS	113.0-261.0	5	3
Santa Rosa, CA (A)	1969/10/02	5.6	SS	80.0-113.0	1	2
Santa Rosa, CA (B)	1969/10/02	5.7	SS	78.9-112.0	1	2
Lytte Creek, CA	1970/09/12	5.3	RV	19.7-76.0	5	2
San Fernando, CA	1971/02/09	6.6	RV	2.8-305.0	11	14
Lake Isabella, CA	1971/03/08	4.1	SS	8.9-8.9	1	0
Dear Valley, CA	1972/02/24	4.7	SS	2.5-2.5	1	0
Point Mugu, CA	1973/02/21	5.6	RV	25.0-25.0	0	1
Hollister, CA	1974/11/28	5.2	SS	39.0-39.0	1	0
Oroville, CA	1975/08/01	5.9	SS	9.5-35.8	2	2
Oroville, CA (R)	1975/08/02	5.1	SS	12.7-14.6	0	2
Oroville, CA (S)	1975/08/02	5.2	SS	12.4-15.0	0	2
Oroville, CA (A)	1975/08/03	4.6	SS	8.4-14.9	1	6



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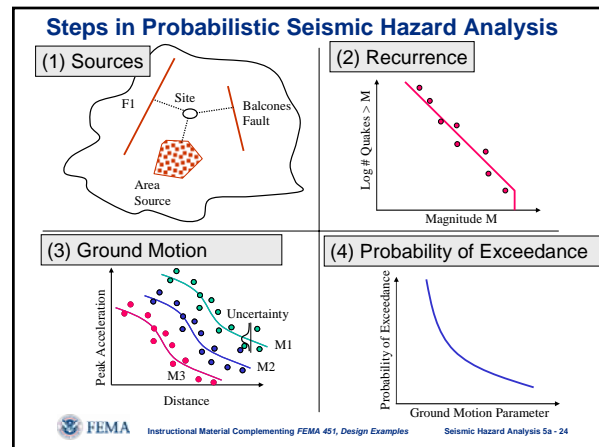
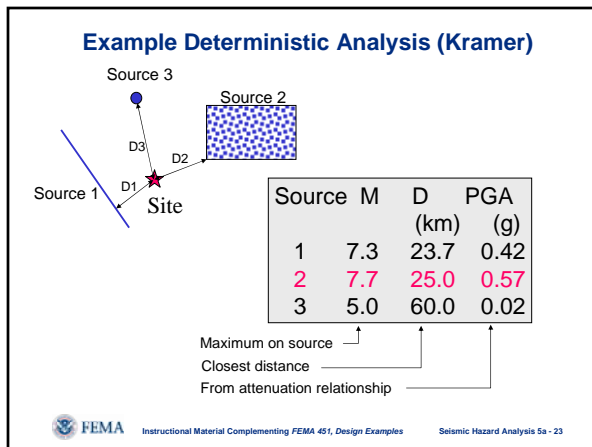
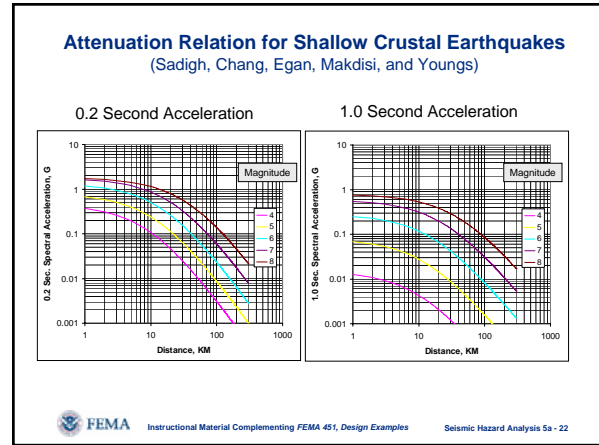
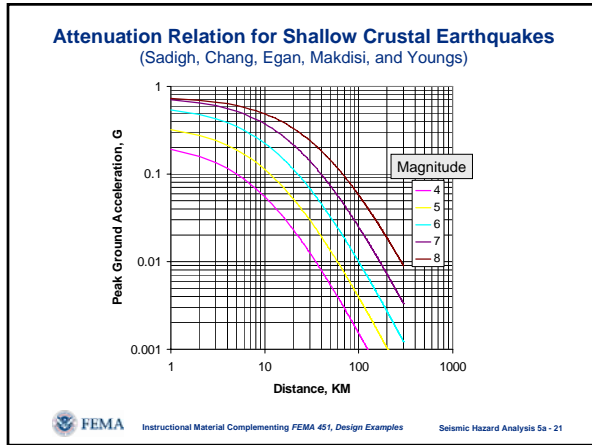
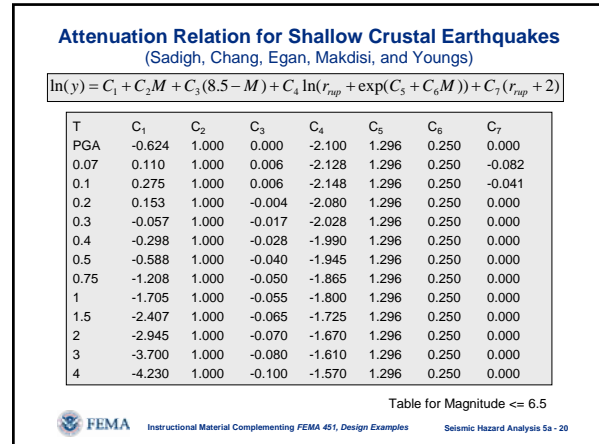
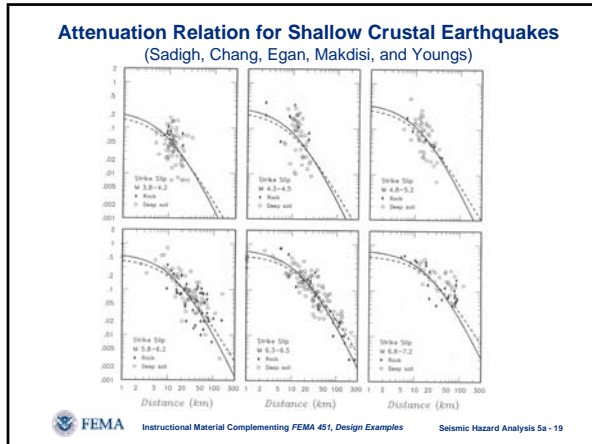
Seismic Hazard Analysis 5a - 17

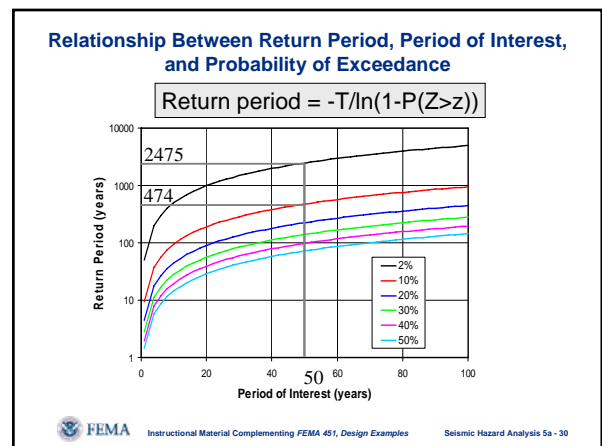
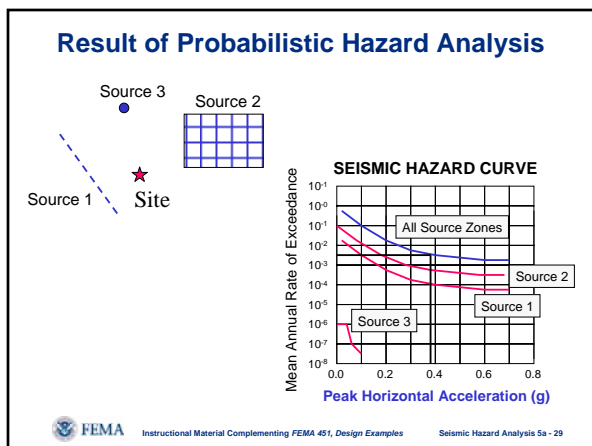
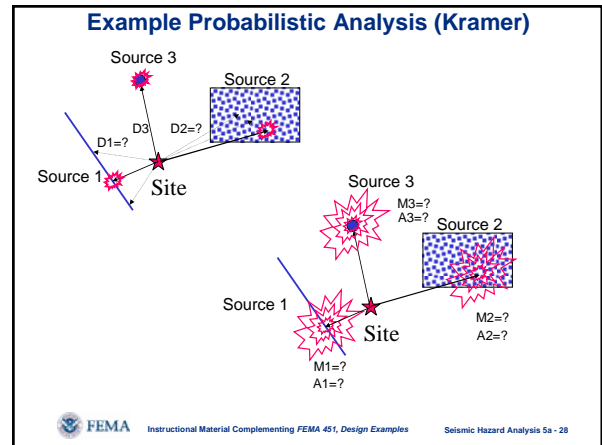
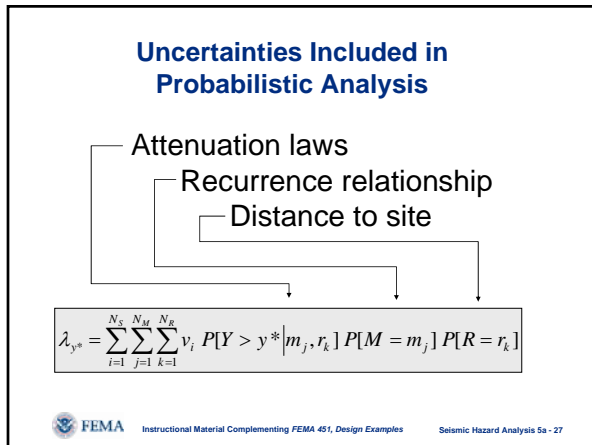
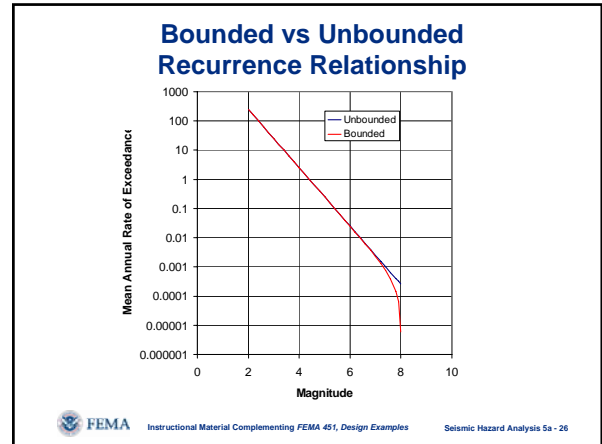
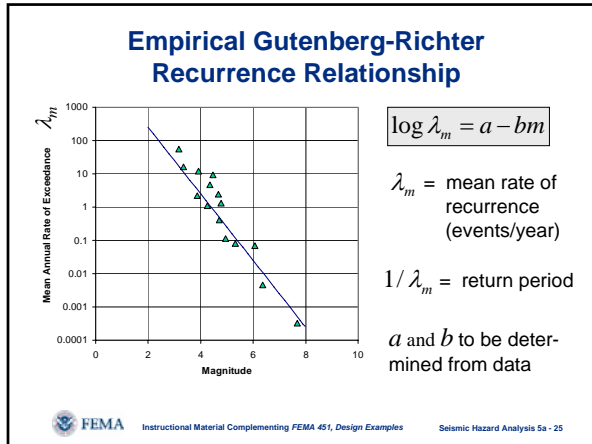
Earthquake Catalog for Shallow Crustal Earthquakes (Sadigh, Chang, Egan, Makdisi, and Youngs)

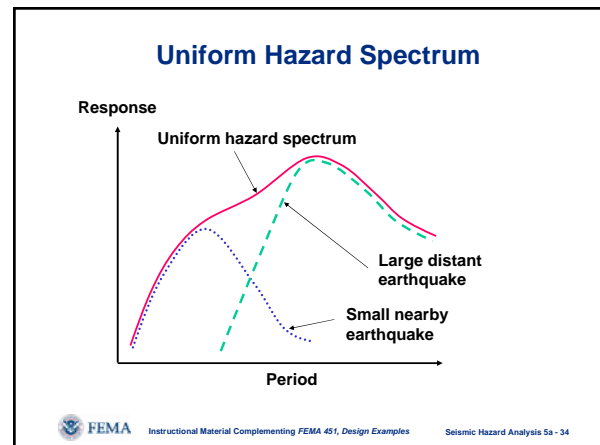
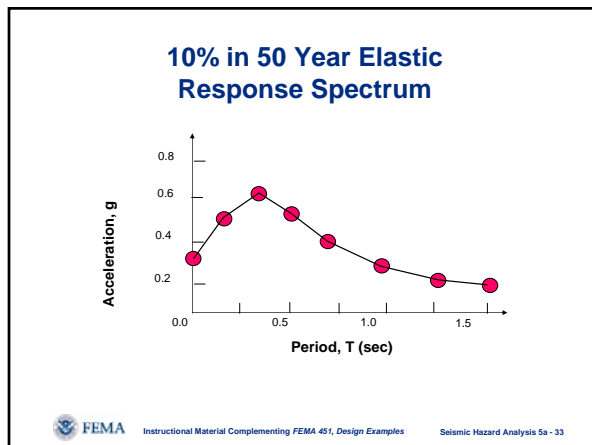
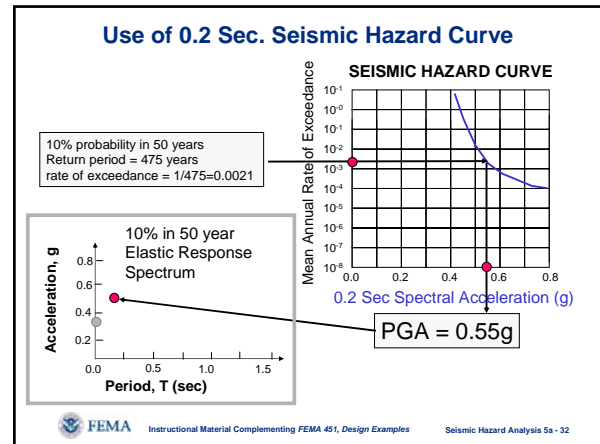
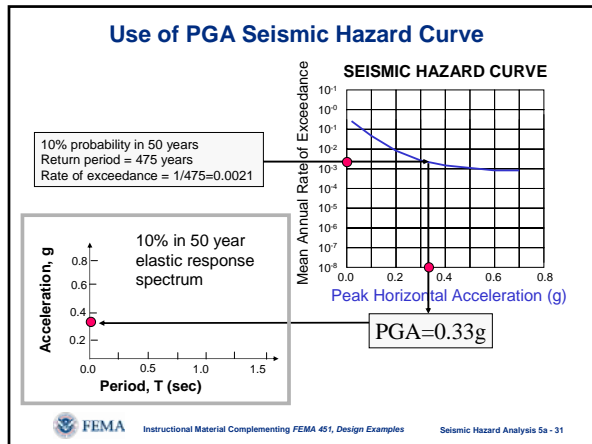


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Uniform Hazard Spectrum

- Developed from *probabilistic* analysis
- All ordinates have equal probability of exceedance
- Represents contributions from small local, large distant earthquakes
- May be overly conservative for modal response spectrum analysis
- May not be appropriate for artificial ground motion generation

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Probabilistic vs Deterministic Seismic Hazard Analysis

"The *deterministic* approach provides a clear and trackable method of computing seismic hazard whose assumptions are easily discerned. It provides understandable scenarios that can be related to the problem at hand."

"However, it has no way for accounting for uncertainty. Conclusions based on deterministic analysis can easily be upset by the occurrence of new earthquakes."

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Probabilistic vs Deterministic Seismic Hazard Analysis

"The *probabilistic* approach is capable of integrating a wide range of information and uncertainties into a flexible framework."

"Unfortunately, its highly integrated framework can obscure those elements which drive the results, and its highly quantitative nature can lead to false impressions of accuracy."

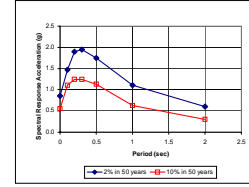
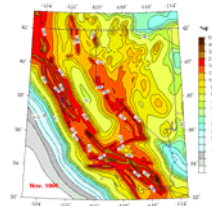


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USGS Probabilistic Hazard Maps (Project 97)

1.0 sec Spectral Acceleration with 1% Probability of Exceedance in 50 Years
vs. NEHRP S-C boundaries



HAZARD MAP

RESPONSE SPECTRA



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USGS Probabilistic Hazard Maps (and NEHRP Provisions Maps)

Earthquake Spectra, Seismic Design Provisions and Guidelines Theme Issue, Volume 16, Number 1, February 2000



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Maximum Considered Earthquake (MCE)

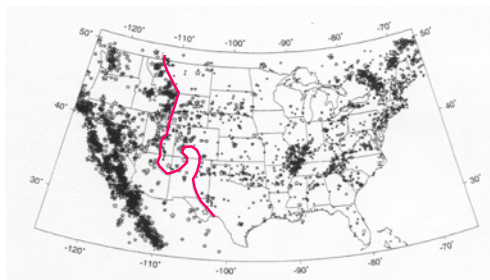
The MCE ground motions are defined as the maximum level of earthquake shaking that is considered as reasonable to design normal structures to resist.



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USGS Seismic Hazard Regions



Note: Different attenuation relationships used for different regions.



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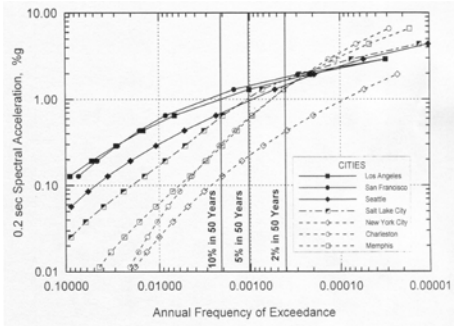
USGS Seismic Hazard WUS Faults



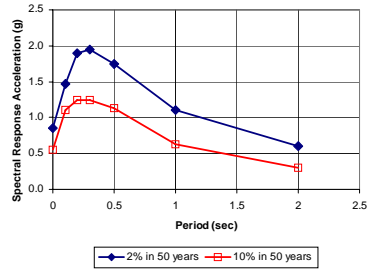
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Seismic Hazard Analysis 5a - 42

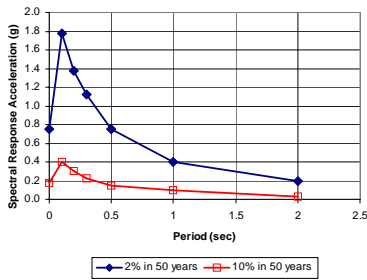
USGS Seismic Hazard Curves for Various Cities



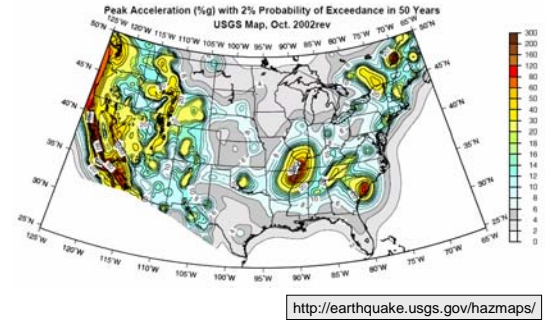
Uniform Hazard Spectra for San Francisco



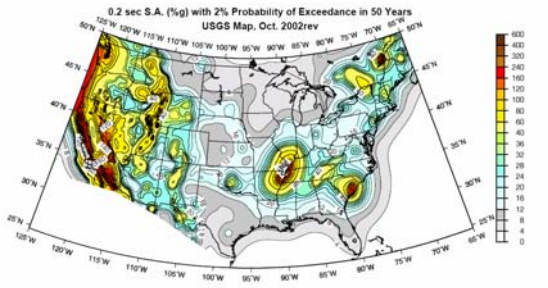
Uniform Hazard Spectra for Charleston, SC



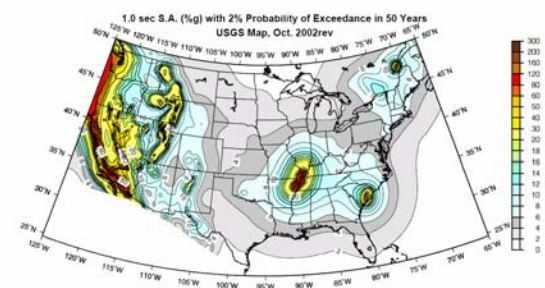
USGS Seismic Hazard Map of Coterminous United States

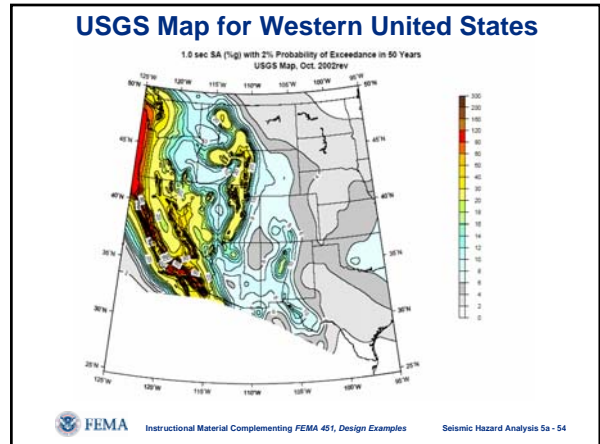
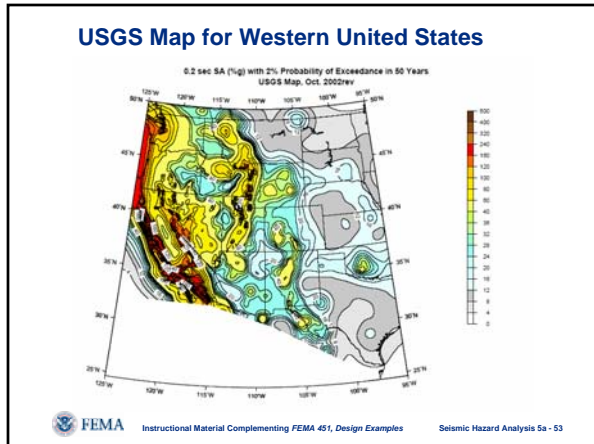
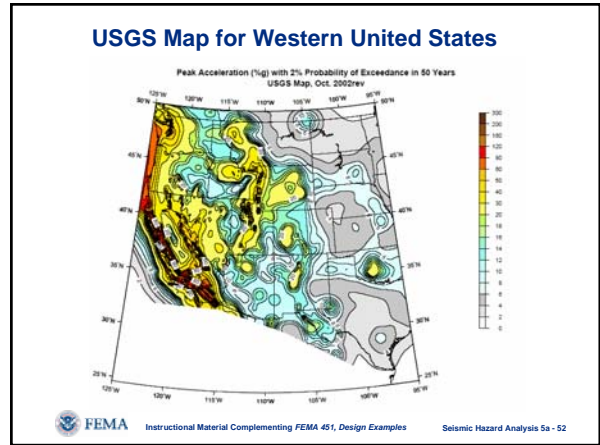
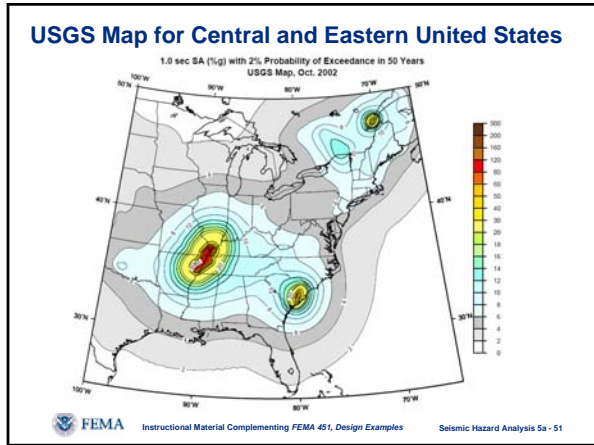
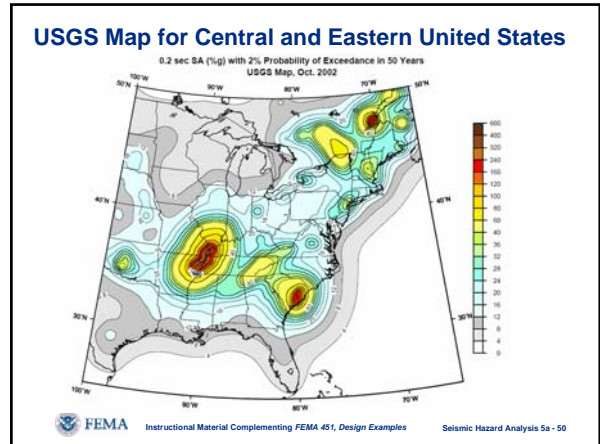
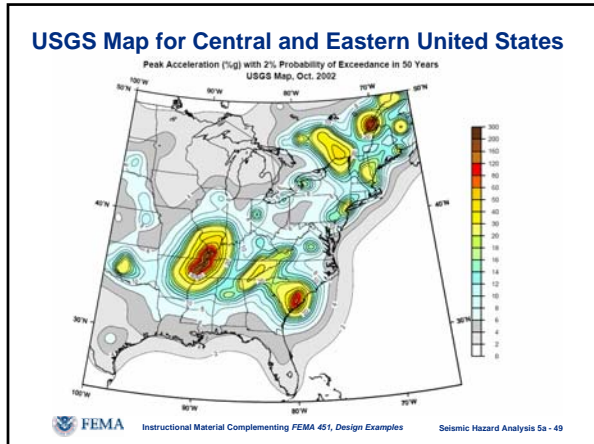


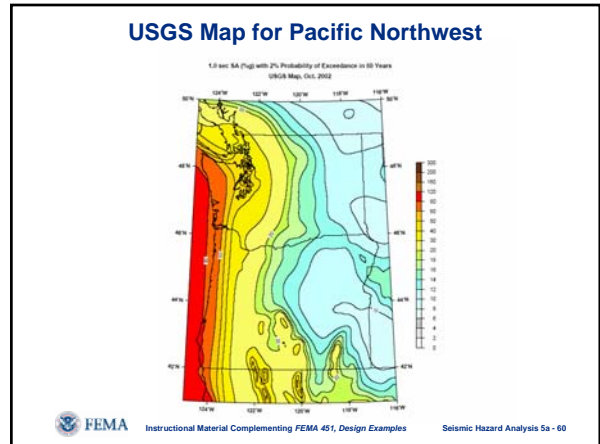
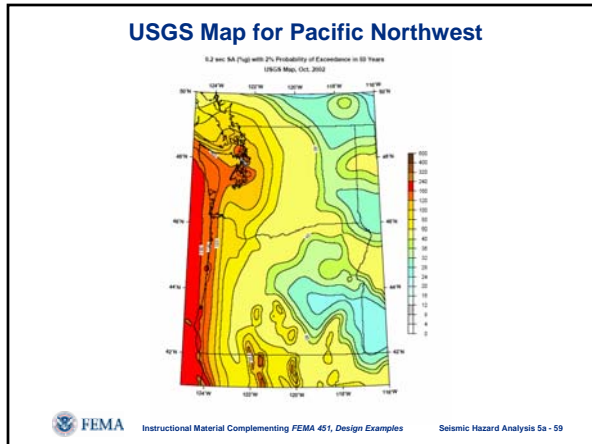
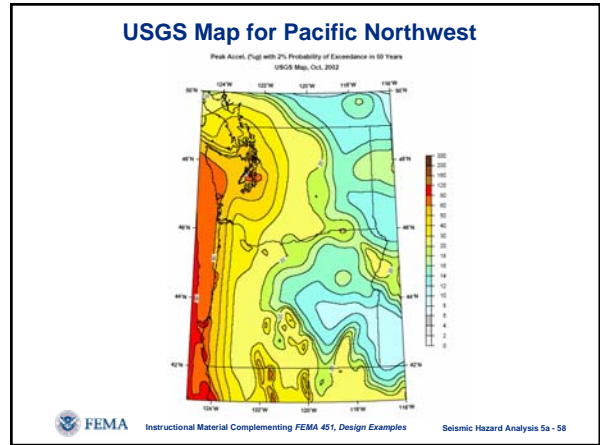
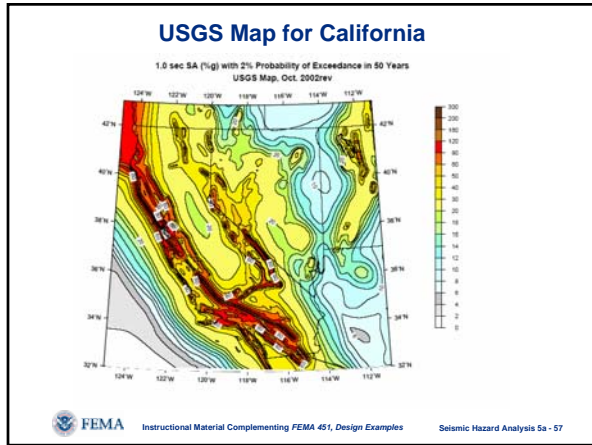
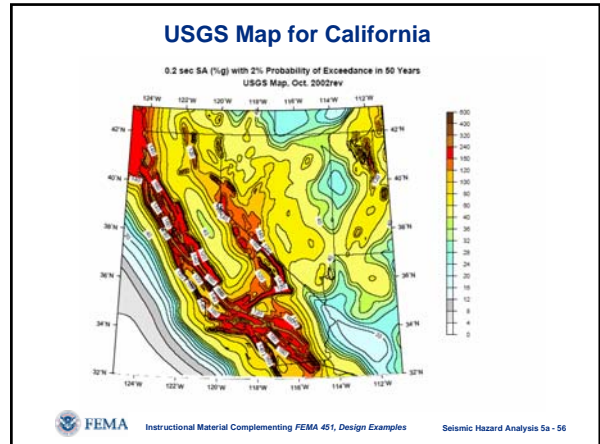
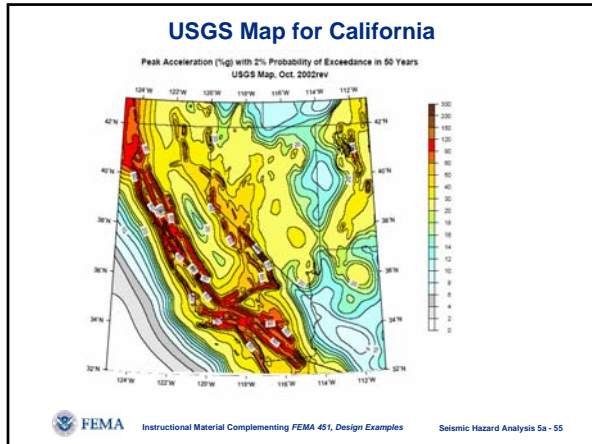
USGS Seismic Hazard Map of Coterminous United States



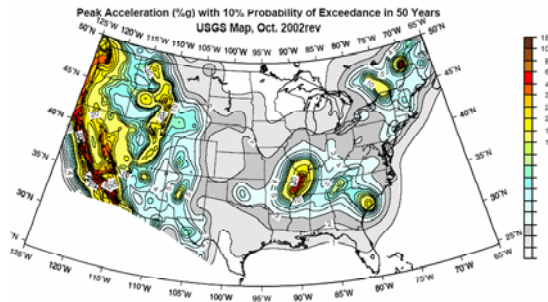
USGS Seismic Hazard Map for Coterminous United States





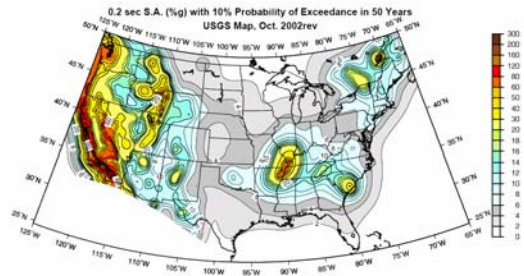


USGS Seismic Hazard Map of Coterminous United States



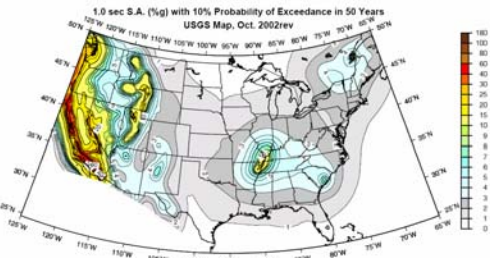
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USGS Seismic Hazard Map of Coterminous United States



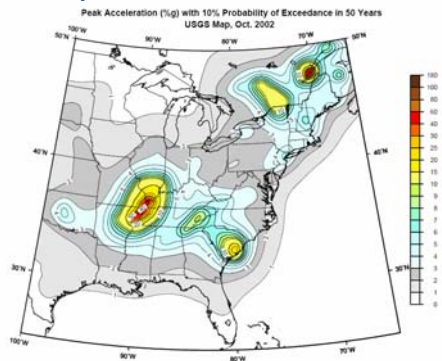
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USGS Seismic Hazard Map of Coterminous United States



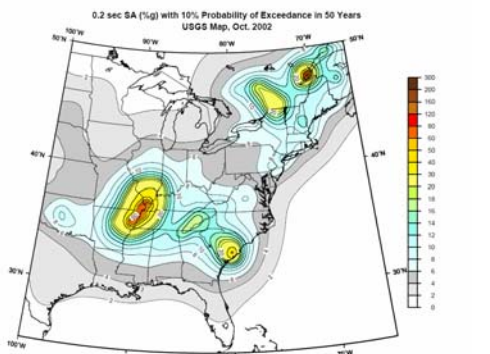
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USGS Map for Central and Eastern United States



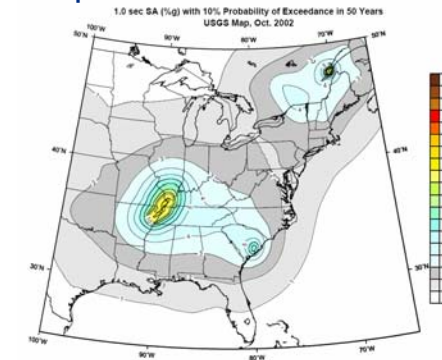
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USGS Map for Central and Eastern United States

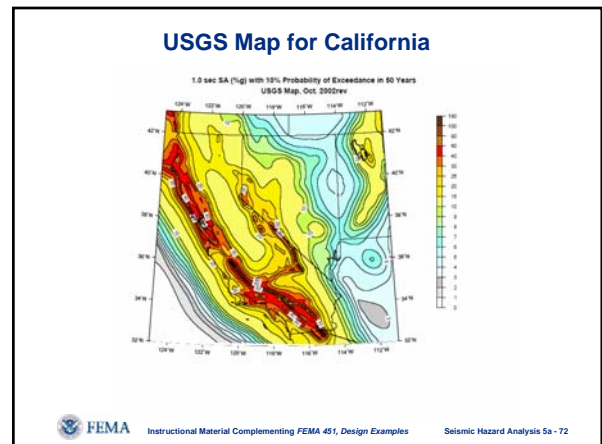
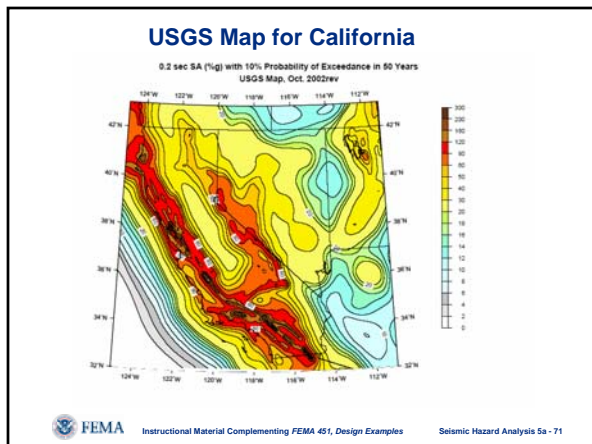
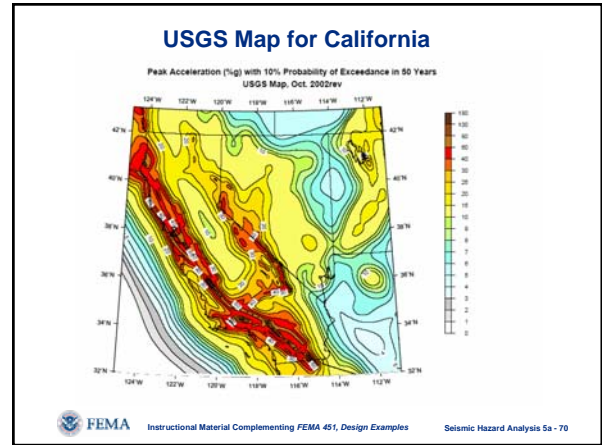
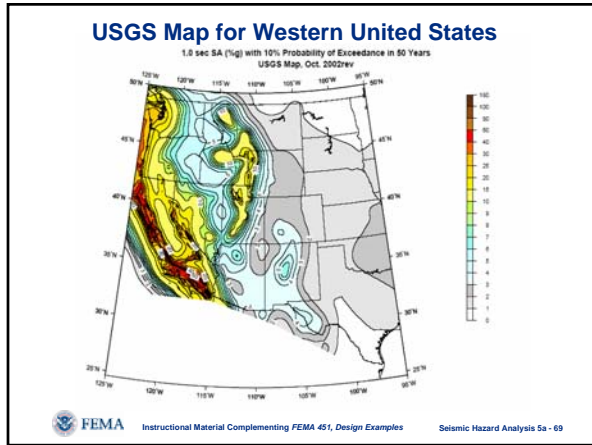
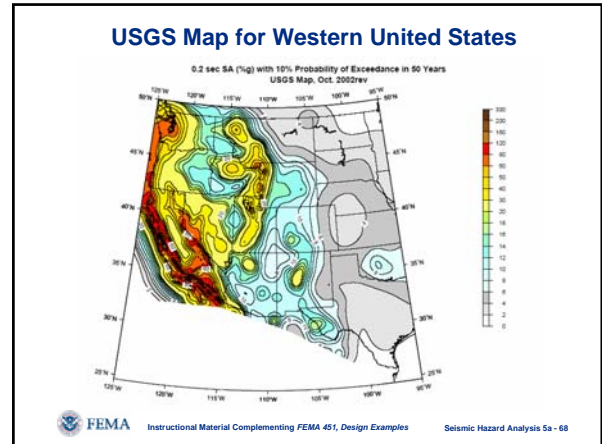
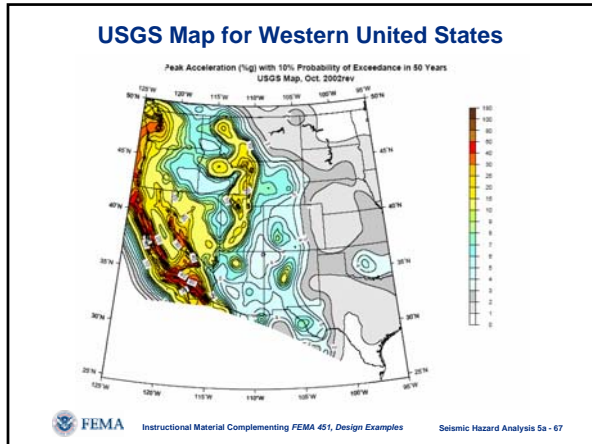


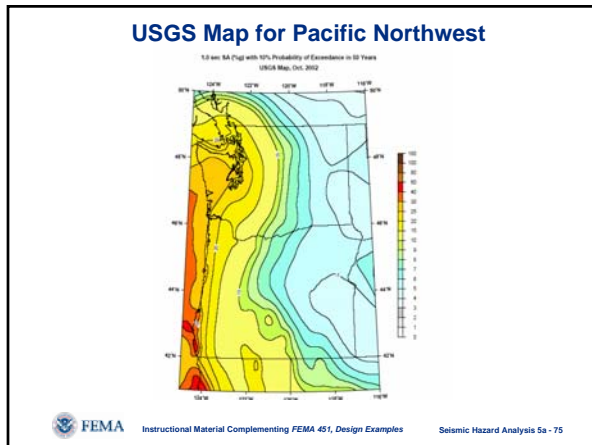
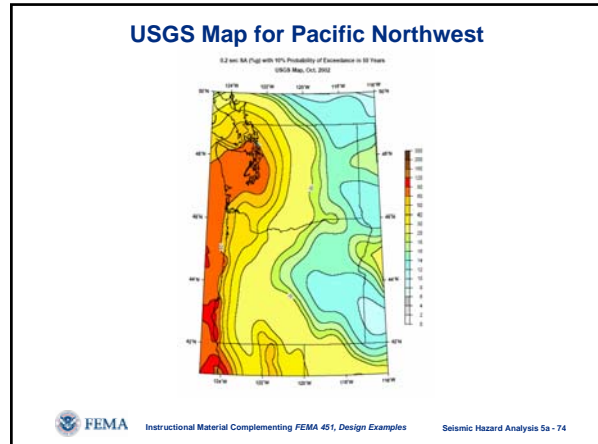
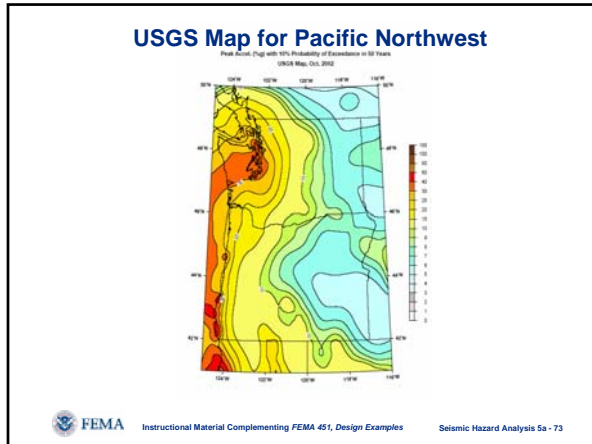
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USGS Map for Central and Eastern United States



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USGS Website for Map Values

<http://earthquake.usgs.gov/research/hazmaps/design/>

The input zipcode is 80203. (DENVER)

ZIP CODE 80203

LOCATION 39.7310 Lat. -104.9815 Long.

DISTANCE TO NEAREST GRID POINT 3.7898 kms

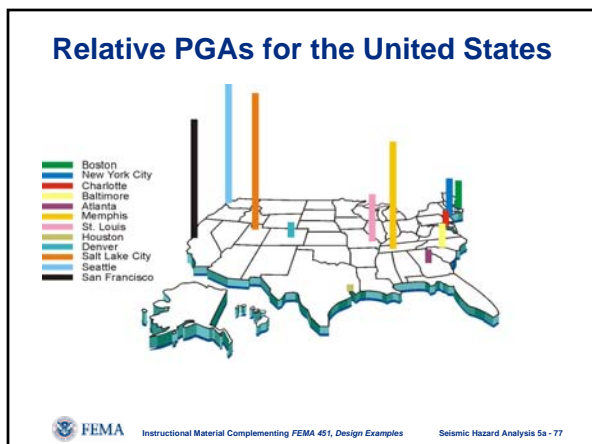
NEAREST GRID POINT 39.7 Lat. -105.0 Long.

Probabilistic ground motion values, in %, at the Nearest Grid point are:

	10%PE in 50 yr	5%PE in 50 yr	2%PE in 50 yr
PGA	3.299764	5.207589	9.642159
0.2 sec SA	7.728900	11.917400	19.921591
0.3 sec SA	6.178438	9.507714	16.133711
1.0 sec SA	2.334019	3.601994	5.879917

CAUTION: USE OF ZIPCODES IS DISCOURAGED; LAT-LONG VALUES WILL GIVE ACCURATE RESULTS.

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2000 NEHRP Recommended Provisions Maps

- 5% damped, 2% in 50 years, Site Class B (firm rock)
- 0.2 second and 1.0 second spectral ordinates provided
- On certain faults in California, Alaska, Hawaii, and CUS Provisions values are deterministic cap times 1.5. Outside deterministic areas, Provisions maps are the same as the USGS maps.
- USGS longitude/latitude and zipcode values are probabilistic MCE. To avoid confusion, ALWAYS use Provisions (adopted by ASCE and IBC) maps for design purposes.

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Location of Deterministic Areas



0.2 sec



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Deterministic Cap

Applies only where probabilistic values exceed highest design values from old (Algermissen and Perkins) maps.

The deterministic procedure for mapping applies:

- For known "active" faults
- Uses characteristic largest earthquake on fault
- Uses 150% of value from median attenuation

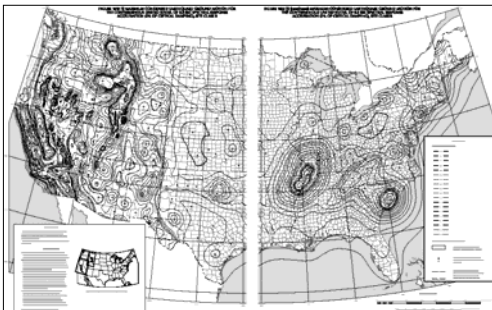
Use deterministic value if lower than 2% in 50 year value



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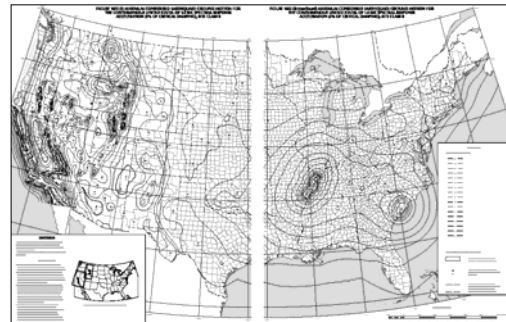
NEHRP Provisions Maps 0.2 Second Spectral Response (S_s)



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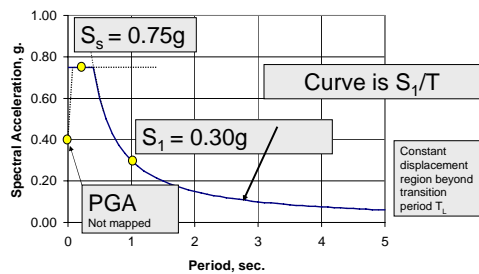
NEHRP Provisions Maps 1.0 Second Spectral Response (S_1)



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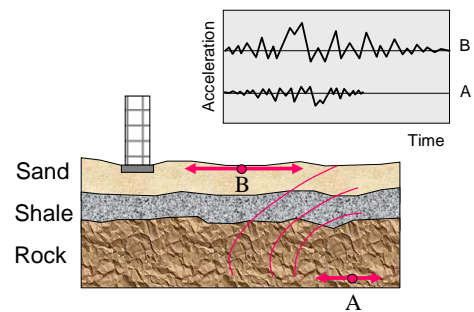
2% in 50 Year 5% Damped MCE Elastic Spectra Site Class B (Firm Rock)



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Site Amplification Effects



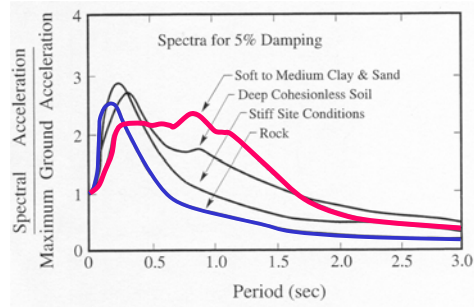
Instructional Material Complementing FEMA 451, Design Examples

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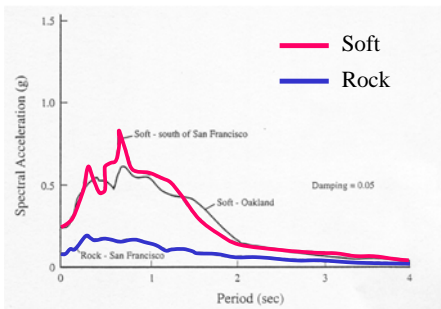
Site Amplification Effects

- Amplification of ground motion
- Longer duration of motion
- Change in frequency content of motion
- Not the same as soil-structure interaction

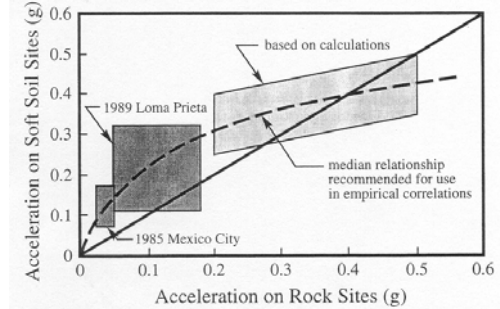
Site Amplification (Seed et al.)



Site Amplification: Loma Prieta Earthquake



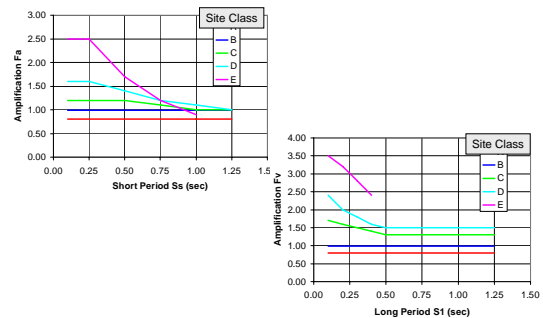
Site Amplification: Loma Prieta and Mexico City Earthquakes



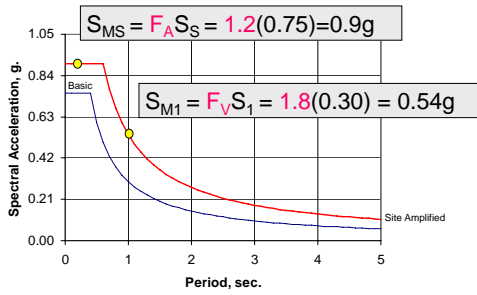
NEHRP Provisions Site Classes

- A** Hard rock $v_s > 5000$ ft/sec
- B** Rock: $2500 < v_s < 5000$ ft/sec
- C** Very dense soil or soft rock: $1200 < v_s < 2500$ ft/sec
- D** Stiff soil : $600 < v_s < 1200$ ft/sec
- E** $v_s < 600$ ft/sec
- F** Site-specific requirements

NEHRP Site Amplification for Site Classes A through E



2% in 50 Year 5% Damped MCE Elastic Spectra Modified for Site Class D



Scaling of NEHRP Provisions Spectra by 2/3 for "Margin of Performance"

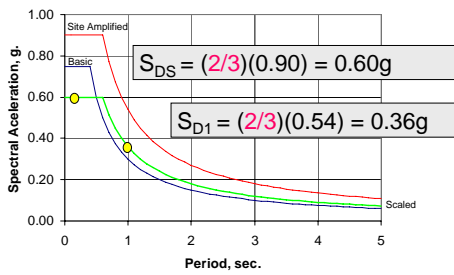
Buildings designed according to current procedures assumed to have margin of collapse of 1.5

Judgment of "lower bound" margin of collapse given by current design procedures

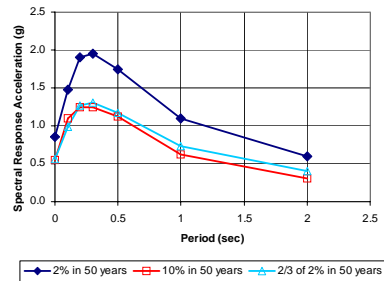
Design with current maps (2% in 50 year) but scale motions by 2/3

Results in $2/3 \times 1.5 = 1.0$ deterministic earthquake (where applicable)

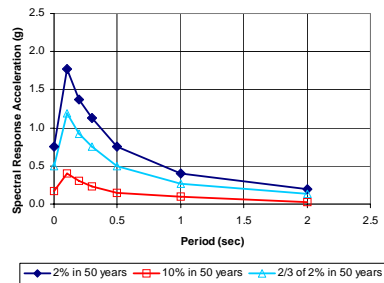
2% in 50 Year 5% Damped Elastic Design Spectra (Scaled by 2/3)



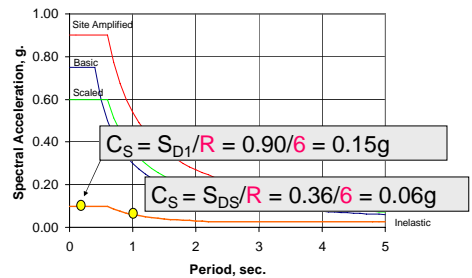
Effect of Scaling in Western United States



Effect of Scaling in Eastern United States



2% in 50 Year 5% Damped Inelastic Design Spectra (R=6, I=1) Site Class D



Basis for Reduction of Elastic Spectra by R

Inelastic behavior of structures

Methods for obtaining acceptable inelastic response are presented in later topics

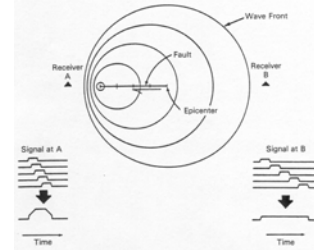


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Directionality and "Killer Pulse" Earthquakes

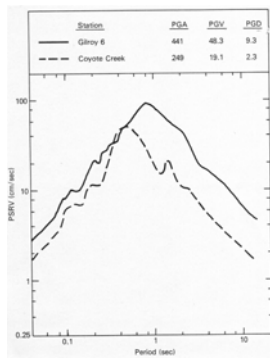
For sites relatively close to the fault, the direction of fault rupture can have an amplifying effect on ground motion amplitude.



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Effect of Directionality on Response Spectra



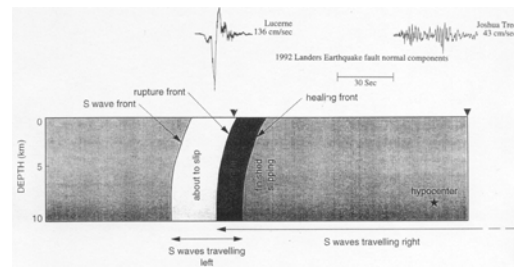
ards



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Effect of Directionality on Ground Motion



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Seismic Hazard Analysis 5a - 100