### 4.8. Method of transformed Sections

- a. Limited to consideration of sections in which concrete stress-strain is linear.
- b. Applicable to either sections in bending or axial compression.
- c. Knowledge or assumption about the depth of cracking of the section is required.
- d. General examination of the method



# **4.9. Method of Transformed Section for Beams:**

## 4.9.1. Uncracked Sections (Cracked Moment, Mcr)

Applicable to beams uncracked section when  $0 < M < M_{cr}$  (where  $M_{cr}$  is the crack moment)



### 4.9.2. Cracked Sections

Applicable to beams cracked section when  $M_{cr} < M < M_y$  (where  $M_y$  is the yield moment)



# 4.10. Example of Transformed Section Applied to Beam

 Consider the section shown below. Calculate the stress caused by a bending moment of 13.83 ft-kips.

$$f'_c = 5 \text{ ksi}$$
  
 $f_y = 60 \text{ ksi}$   
 $f_r = 500 \text{ psi}$ 

Section Properties:

$$A_{s} = 3 - \#6 \ bars$$

$$A_{s} = 3 \times 0.44 \ (in^{2}) = 1.32 \ in^{2}$$

$$E_{c} = 57,000 \sqrt{5,000} = 4.03 \times 10^{6} \ psi$$

$$n = \frac{29,000,000 \ psi}{4.03 \times 10^{6} \ psi} = 7.2 \rightarrow use \ n = 7$$

$$\rho = \frac{A_{s}}{bd} = \frac{1.32 \ in^{2}}{8 \ (in) \times 12 \ (in)} = 0.014$$



## For Uncracked Section (Assume)

Find the location of neutral axis (First Moment of Area = 0).

$$(8\overline{y})\left(\frac{\overline{y}}{2}\right) = 8(15 - \overline{y}) \times \left(\frac{15 - \overline{y}}{2}\right) + (12 - \overline{y})(7.92)$$

$$\overline{y} = 7.78 \text{ in}$$
or find the centroid of the cross section by using the top edge as the reference point.
$$\overline{y} = \frac{8 \times 15 \times \frac{15}{2} + 7.92 \times 12}{8 \times 15 + 7.92}$$

$$\overline{y} = 7.78 \text{ in}$$

$$Area of overhangs; (n - 1)A_s = 6 \times 1.32 = 7.92 \text{ in}^2$$

This value (7.78 in) should be the same as the one we get using Eq. (4.2) found earlier. (see next page for proof).

$$\frac{c}{d} = \frac{2\rho(n-1) + (h/d)^2}{2\rho(n-1) + 2(h/d)}$$
(4.2)

Substitute

$$\frac{c}{d} = \frac{2(0.014)(7 - 1) + (15/12)^2}{2(0.014)(7 - 1) + 2(15/12)} = 0.65$$

Solve for *c* 

$$\rightarrow \frac{c}{d} = 0.65$$
 therefore  $c = 0.65d = 7.78$  in

#### Note:

For a homogenous section, we can relate bending moment to stresses at distance "y" from the neutral axis as the following

$$f = M\frac{Y}{I}$$

where

f = stress
 M = bending moment
 y = distance from neutral axis to the point where stresses are to be calculated
 I = moment of inertia of the cross section

# Calculate *I<sub>n.a.</sub>*

$$I_{NA.} = \frac{1}{3} \times 8 \times 7.78^3 + \frac{1}{3} \times 8 \times (15 - 7.78)^3 + 7.92 \times (12 - 7.78)^2$$
$$I_{NA.} = 2,400 \ (in^4)$$

### **Calculate stresses**

Now, find the stress in top fiber (compression stress at top fiber):

$$f_{top} = \frac{M\bar{y}}{I_{NA.}} = \frac{(13.83 \ ft - kips) \times (12 \ in/ft) \times (7.78 \ in)}{2,400 \ in^4} = 0.54 \ k/in^2$$
  
$$f_{bot} = \frac{M(15 - \bar{y})}{I_{NA.}} = \frac{(13.83 \ ft - kips) \times (12 \ in/ft) \times (15 \ -7.78 \ in)}{2,400 \ in^4} = 0.50 \ k/in^2$$
  
$$f_{bot} = 0.50 \ k/in^2 \le f_r = 0.5 \ ksi$$

Therefore, the assumption of uncracked section was correct, since tension stresses are smaller than  $f_r$  given in the problem.

### 4.11. Example 2. Calculate Yield Moment for the Beam

Assume concrete accepts no tension. (yield moment is when steel is starting to yield). Locate N.A.



Calculate *I<sub>n.a.</sub>* 

$$I_{NA.} = \frac{1}{3} \times 8 \times 4.24^3 + 9.24 \times 7.76^2$$
  
 $I_{NA.} = 760 in^4$ 

At level of steel, if  $f_y = 60,000$  psi, then the stress in the transformed section will be

$$\frac{f_y}{n} = \frac{60,000}{7} = 8,570 \ psi$$

and

$$M = \frac{fI}{y} = \frac{(8,570 \text{ psi})(760 \text{ in}^4)}{7.76 \text{ in}} = 839,000 \text{ in} - lb = 839 \text{ in} - kips$$

See next page for check with previous methods that we have learned.

# Check

Check the moment found in the previous page with Eq. :

$$k = \sqrt{(\rho n)^2 + 2\rho n} - \rho n$$

$$k = \sqrt{(0.014 \times 7)^2 + 2(0.014)(7)} - (0.014)(7)$$

$$k = 0.355$$

$$(4.3)$$

therefore

$$kd = 0.355(12) = 4.22 in$$

this is very close to what we calculated for  $\overline{y} = 4.24$  in the last page. The slight difference is due to significant digit calculations.

Therefore

$$M_y = A_s f_y d(1 - \frac{k}{3}) = (1.32 in^2)(60 ksi)(12 in)(1 - \frac{0.355}{3})$$

 $M_y = 838 \text{ in-kips}$