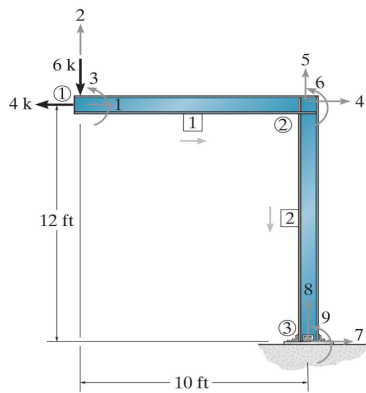


Problem 16a-1



Element 1

L =

120

in

I =

650

in⁴

A =

20

in²

E =

29,000

ksi

θ_x =

0

°

θ_y =

90

°

λ_x =

1.000

λ_y =

0.000

AE/L =

4,833.3

k/in

12EI/L³ =

130.9

k/in

6EI/L² =

7,854.2

k

4EI/L =

628,333.3

k in

2EI/L =

314,166.7

k in

1	2	3	4	5	6	
4,833.33	0.00	0.00	-4,833.33	0.00	0.00	1
0.00	130.90	7,854.17	0.00	-130.90	7,854.17	2
0.00	7,854.17	628,333.33	0.00	-7,854.17	314,166.67	3
-4,833.33	0.00	0.00	4,833.33	0.00	0.00	4
0.00	-130.90	-7,854.17	0.00	130.90	-7,854.17	5
0.00	7,854.17	314,166.67	0.00	-7,854.17	628,333.33	6

Element 2

L =

144

in

I =

650

in⁴

A =

20

in²

E =

29,000

ksi

θ_x =

90

°

θ_y =

180

°

λ_x =

0.000

λ_y =

-1.000

AE/L =

4,027.8

k/in

12EI/L³ =

75.8

k/in

6EI/L² =

5,454.3

k

4EI/L =

523,611.1

16a-1

2EI/L =

261,805.6

k in

4	5	6	7	8	9	
75.75	0.00	5,454.28	-75.75	0.00	5,454.28	4
0.00	4,027.78	0.00	0.00	-4,027.78	0.00	5
5,454.28	0.00	523,611.11	-5,454.28	0.00	261,805.56	6
-75.75	0.00	-5,454.28	75.75	0.00	-5,454.28	7
0.00	-4,027.78	0.00	0.00	4,027.78	0.00	8
5,454.28	0.00	261,805.56	-5,454.28	0.00	523,611.11	9

	1	2	3	4	5	6	7	8	9	
k1	4,833.33	0.00	0.00	-4,833.33	0.00	0.00				1
	0.00	130.90	7,854.17	0.00	-130.90	7,854.17				2
	0.00	7,854.17	628,333.33	0.00	-7,854.17	314,166.67				3
	-4,833.33	0.00	0.00	4,833.33	0.00	0.00				4
	0.00	-130.90	-7,854.17	0.00	130.90	-7,854.17				5
	0.00	7,854.17	314,166.67	0.00	-7,854.17	628,333.33				6
										7
										8
										9

	1	2	3	4	5	6	7	8	9	
k2										1
										2
										3
				75.75	0.00	5,454.28	-75.75	0.00	5,454.28	4
				0.00	4,027.78	0.00	0.00	-4,027.78	0.00	5
				5,454.28	0.00	523,611.11	-5,454.28	0.00	261,805.56	6
				-75.75	0.00	-5,454.28	75.75	0.00	-5,454.28	7
				0.00	-4,027.78	0.00	0.00	4,027.78	0.00	8
				5,454.28	0.00	261,805.56	-5,454.28	0.00	523,611.11	9

	1	2	3	4	5	6	7	8	9	
K	4833.33	0.00	0.00	-4833.33	0.00	0.00	0.00	0.00	0.00	1
	0.00	130.90	7854.17	0.00	-130.90	7854.17	0.00	0.00	0.00	2
	0.00	7854.17	628333.33	0.00	-7854.17	314166.67	0.00	0.00	0.00	3
	-4833.33	0.00	0.00	4909.09	0.00	5454.28	-75.75	0.00	5454.28	4
	0.00	-130.90	-7854.17	0.00	4158.68	-7854.17	0.00	-4027.78	0.00	5
	0.00	7854.17	314166.67	5454.28	-7854.17	1151944.44	-5454.28	0.00	261805.56	6
	0.00	0.00	0.00	-75.75	0.00	-5454.28	75.75	0.00	-5454.28	7
	0.00	0.00	0.00	0.00	-4027.78	0.00	0.00	4027.78	0.00	8
	0.00	0.00	0.00	5454.28	0.00	261805.56	-5454.28	0.00	523611.11	9

	1	2	3	4	5	6	
K	4833.33	0.00	0.00	-4833.33	0.00	0.00	1
	0.00	130.90	7854.17	0.00	-130.90	7854.17	2
	0.00	7854.17	628333.33	0.00	-7854.17	314166.67	3
	-4833.33	0.00	0.00	4909.09	0.00	5454.28	4
	0.00	-130.90	-7854.17	0.00	4158.68	-7854.17	5
	0.00	7854.17	314166.67	5454.28	-7854.17	1151944.44	6

Q	
-4	1
-6	2
0	3
0	4
0	5
0	6

D = K ⁻¹ Q	
-0.60806	in.
-1.10888	in.
0.00999	radians
-0.60723	in.
-0.00149	in.
0.00770	radians

	1	2	3	4	5	6	7	8	9	
K	4833.33	0.00	0.00	-4833.33	0.00	0.00	0.00	0.00	0.00	1
	0.00	130.90	7854.17	0.00	-130.90	7854.17	0.00	0.00	0.00	2
	0.00	7854.17	628333.33	0.00	-7854.17	314166.67	0.00	0.00	0.00	3
	-4833.33	0.00	0.00	4909.09	0.00	5454.28	-75.75	0.00	5454.28	4
	0.00	-130.90	-7854.17	0.00	4158.68	-7854.17	0.00	-4027.78	0.00	5
	0.00	7854.17	314166.67	5454.28	-7854.17	1151944.44	-5454.28	0.00	261805.56	6
	0.00	0.00	0.00	-75.75	0.00	-5454.28	75.75	0.00	-5454.28	7
	0.00	0.00	0.00	0.00	-4027.78	0.00	0.00	4027.78	0.00	8
	0.00	0.00	0.00	5454.28	0.00	261805.56	-5454.28	0.00	523611.11	9

D	Q	
-0.60806	-4.00	
-1.10888	-6.00	
0.00999	0.00	
-0.60723	0.00	
-0.00149	0.00	
0.00770	0.00	
0.00000	4.00	k
0.00000	6.00	k
0.00000	-1296.00	k-in