

Calvin: I think night time is dark so you can imagine your fears with less distraction.



- o The first slide is not a homework problem.
- There are two homework problems and the second homework problem is on the last two slides.



 When we first considered the Bernoulli expression with a pump in the system we wrote the expression as

$$gz_1 + \frac{v_1^2}{2} + \frac{p_1}{\rho} + e_{pump} = gz_2 + \frac{v_2^2}{2} + \frac{p_2}{\rho}$$



o When we look at the expression in terms of pressure

$$\rho g z_1 + \frac{\rho v_1^2}{2} + p_1 + \rho e_{pump} = \rho g z_2 + \frac{\rho v_2^2}{2} + p_2$$



o And add in the loss terms

$$\rho g z_1 + \frac{\rho v_1^2}{2} + \rho_1 + \rho e_{pump} + Friction + Minor = \rho g z_2 + \frac{\rho v_2^2}{2} + \rho_2$$



o Substituting the forms we developed

$$\rho g z_1 + \frac{\rho v_1^2}{2} + \rho_1 + \rho e_{pump} - \sum \frac{fL}{d} \frac{\rho v^2}{2} - \sum K \frac{\rho v^2}{2} = \rho g z_2 + \frac{\rho v_2^2}{2} + \rho_2$$



- To get the form in terms of energy we divide by the density and multiply by the mass flow rate
- o I am also collecting terms on the right side.

$$-\frac{dW}{dt}_{pump} = \dot{m}\left(gz_{2} + \frac{v_{2}^{2}}{2} + \frac{p_{2}}{\rho} - gz_{1} - \frac{v_{1}^{2}}{2} - \frac{p_{1}}{\rho} + \sum\frac{fL}{d}\frac{v^{2}}{2} + \sum\frac{v^{2}}{2}\right)$$



• A house is located near a freshwater lake. The homeowner decides to install a pump near the lake to deliver 25 gpm of water to a tank adjacent to the house. The water can then be used for lavatory facilities or sprinkling the lawn. For the system sketched in Figure 5.31, determine the pump power required.





• Dr. Janna chooses to look at the problem in three parts. This is really not necessary. We can look at the points labeled 1 and 4 and work through the problem.

At point 1

 $v_{1} \coloneqq 0 \frac{\text{ft}}{\text{s}} \qquad z_{1} \coloneqq 0 \text{ft} \qquad p_{1} \coloneqq 0 \frac{\text{lbf}}{\text{ft}^{2}}$ At point 2 $v_{4} \coloneqq 0 \frac{\text{ft}}{\text{s}} \qquad z_{4} \coloneqq 30 \text{ft} \qquad p_{4} \coloneqq 0 \frac{\text{lbf}}{\text{ft}^{2}}$



o Considering the fluid

For the entire system

$$Q := 25 \frac{\text{gal}}{\text{min}} = 0.056 \frac{\text{ft}^3}{\text{s}}$$

$$\rho \coloneqq 1.94 \frac{\text{slug}}{\text{ft}^3} \qquad \qquad \mu \coloneqq 1.9 \cdot 10^{-5} \frac{\text{lbf} \cdot \text{s}}{\text{ft}^2}$$



• And the pipe characteristics

And the characteristics of the pipe

$$d := 0.125 \text{ft} \qquad A := \pi \cdot \frac{d^2}{4} = 0.012 \text{ ft}^2$$
$$L := 115 \text{ft} \qquad \varepsilon := 0 \text{ft}$$



Calculating the velocity in the pipe and the friction factor.

$$\mathbf{v} \coloneqq \frac{\mathbf{Q}}{\mathbf{A}} = 4.539 \, \frac{\mathrm{ft}}{\mathrm{s}}$$

$$\operatorname{Re} := \frac{\rho \cdot \mathbf{v} \cdot \mathbf{d}}{\mu} = 5.793 \times 10^4$$

Flow is Turbulent

$$f := \frac{0.25}{\log \left(\frac{\varepsilon}{3.7 \cdot d} + \frac{5.74}{Re^{0.9}}\right)^2} = 0.02$$



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So the friction loss is

$$\text{Loss}_{\text{friction}} \coloneqq \frac{\mathbf{f} \cdot \mathbf{L}}{d} \cdot \frac{\mathbf{v}^2}{2} = 17.686 \frac{\mathbf{m}^2}{\frac{2}{s^2}}$$

 $\text{Loss}_{\text{friction}} \cdot \rho \cdot Q = 0.037 \text{ hp}$



And the minor losses

$$K_{\text{strainer}} \coloneqq 1.3 \qquad K_{45} \coloneqq 0.35 \qquad K_{90} \coloneqq 0.31 \qquad K_{\text{exit}} \coloneqq 1$$

$$\text{Loss}_{\text{minor}} \coloneqq \left(K_{\text{strainer}} + 2 \cdot K_{45} + 3 \cdot K_{90} + K_{\text{exit}} \right) \cdot \frac{v^2}{2} = 40.482 \frac{\text{ft}^2}{s^2}$$

$$\text{Loss}_{\text{minor}} \cdot \rho \cdot Q = 7.953 \times 10^{-3} \text{ hp}$$



For the system

$$Pump_{power} := -\rho \cdot Q \cdot \left(g \cdot z_4 + \frac{v_4^2}{2} + \frac{p_4}{\rho} - g \cdot z_1 - \frac{v_1^2}{2} - \frac{p_1}{\rho} + Loss_{friction} + Loss_{minor} \right) = -0.235 \text{ hp}$$

$$+Pump_{power} = -129.246 \frac{\text{ft} \cdot \text{lbf}}{8}$$



In a dairy products processing plant, milk (ρ = 030 kg/m³, μ =2.12×10⁻³ N s/m²) is pumped through a piping system from a tank to a container packaging machine. The pump and piping are all stainless steel (smooth walled), arranged as shown in Figure P5.71. The pump inlet line (4-nominal, schedule 40 pipe) is 2 m long. The pump outlet line (3 1/2-nominal, schedule 40 pipe) is 15 m long. All fittings are flanged, and the flow rate through the system is 0.015 m³/s. Determine the electrical power input to the pump if the pump-motor efficiency is 88%.





At point 1 which is the top of the tank.

$$v_1 := 0 \frac{ft}{s}$$
 $z_1 := 0 ft$ $p_1 := 0 \frac{lbf}{ft^2}$

At point 2 which is the top of the container.

$$v_2 \coloneqq 0 \frac{ft}{s}$$
 $z_2 \coloneqq 6m$ $p_2 \coloneqq 0 \frac{lbf}{ft^2}$



For the entire system





And the characteristics of the pipes. Point 3 is the pump.

$$d_{1to3} \coloneqq 4.026in = 0.102 \text{ m} \qquad A_{1to3} \coloneqq \pi \cdot \frac{d_{1to3}^2}{4} = 8.213 \times 10^{-3} \text{ m}^2$$
$$d_{3to2} \coloneqq 3.548in = 0.09 \text{ m} \qquad A_{3to2} \coloneqq \pi \cdot \frac{d_{3to2}^2}{4} = 6.379 \times 10^{-3} \text{ m}^2$$
$$L_{1to3} \coloneqq 2m \qquad L_{3to2} \coloneqq 15m \qquad L_{00} \text{ ked both the diameters}$$

 $\varepsilon := 0.015 \cdot 10^{-3} \text{m} = 1.5 \times 10^{-5} \text{m}$

I looked both the diameters and the relative roughness on the internet.



Calculating the velocity in the pipes and the friction factors.

$$v_{1to3} \coloneqq \frac{Q}{A_{1to3}} = 1.826 \frac{m}{s} \qquad v_{3to2} \coloneqq \frac{Q}{A_{3to2}} = 2.352 \frac{m}{s}$$

$$\operatorname{Re}_{1to3} \coloneqq \frac{\rho \cdot v_{1to3} \cdot d_{1to3}}{\mu} = 9.074 \times 10^{4}$$
Flow is Turbulent

$$\operatorname{Re}_{3to2} \coloneqq \frac{\rho \cdot v_{3to2} \cdot d_{3to2}}{\mu} = 1.03 \times 10^5$$
 Flow is Turbulent



So the friction loss is

$$\text{Loss}_{\text{friction}} \coloneqq \frac{f_{1\text{to}3} \cdot L_{1\text{to}3}}{d_{1\text{to}3}} \cdot \frac{v_{1\text{to}3}^2}{2} + \frac{f_{3\text{to}2} \cdot L_{3\text{to}2}}{d_{3\text{to}2}} \cdot \frac{v_{3\text{to}2}^2}{2} = 9.238 \frac{\text{m}^2}{\text{s}^2}$$

 $\text{Loss}_{\text{friction}} \cdot \rho \cdot Q = 142.73 \text{ W}$



So the friction loss is

$$\text{Loss}_{\text{friction}} \coloneqq \frac{f_{1\text{to}3} \cdot L_{1\text{to}3}}{d_{1\text{to}3}} \cdot \frac{v_{1\text{to}3}^2}{2} + \frac{f_{3\text{to}2} \cdot L_{3\text{to}2}}{d_{3\text{to}2}} \cdot \frac{v_{3\text{to}2}^2}{2} = 9.238 \frac{\text{m}^2}{\text{s}^2}$$

 $\text{Loss}_{\text{friction}} \cdot \rho \cdot Q = 142.73 \text{ W}$



And the minor losses

On the left side there is a strainer and a 90 degree bend. On the right side (3 to 2), there is a 90 degree bend, a check valve, and an exit.

 $K_{strainer} \approx 1.3$ $K_{90} \approx 0.31$ $K_{valve} \approx 2.5$ $K_{exit} \approx 1$

$$\text{Loss}_{\text{minor}} := \left(K_{\text{strainer}} + K_{90} \right) \cdot \frac{v_{1\text{to}3}^2}{2} + \left(K_{\text{valve}} + K_{90} + K_{\text{exit}} \right) \cdot \frac{v_{3\text{to}2}^2}{2} = 13.22 \frac{\text{m}^2}{\text{s}^2}$$

 $\text{Loss}_{\text{minor}} \cdot \rho \cdot Q = 204.249 \text{ W}$



For the system

$$Pump_{power} \coloneqq \left[-\rho \cdot Q \cdot \left(g \cdot z_2 + \frac{v_2^2}{2} + \frac{p_2}{\rho} - g \cdot z_1 - \frac{v_1^2}{2} - \frac{p_1}{\rho} + \text{Loss}_{friction} + \text{Loss}_{minor} \right) \right]$$

 $Pump_{power} = -1256.1 W$



At 88% effeciency

$$Pump_{power} := \frac{Pump_{power}}{0.88} = -1.427 \, kW$$



In the first example problem shown in class if the pump in the system is replaced by a pump delivering 0.5 hp, what would the flow rate in the system be?



In the first example problem, if the homeowner wanted to increase the flow in the system by a factor of 4 (4 times the flow of the original problem) and decided to by a pump with 4x the power of the original system, what percentage of their desired flow rate would they achieve?



Octane is to be pumped overland in a piping system. The octane is routed from storage tanks to the main pump by smaller pumps. One such arrangement is sketched in Figure shown. This pump must supply 0.4 m3/s of octane to the main pump. All fittings are flanged; the pipe is cast iron, schedule 160, 24-nominal, with L=65 m. The absolute pressure at section 2 is 282.5 kPa. Determine the power required to be transferred to the liquid. Assuming an overall pump-motor efficiency of 75%, determine the input power required by the motor.



Piping System Problems