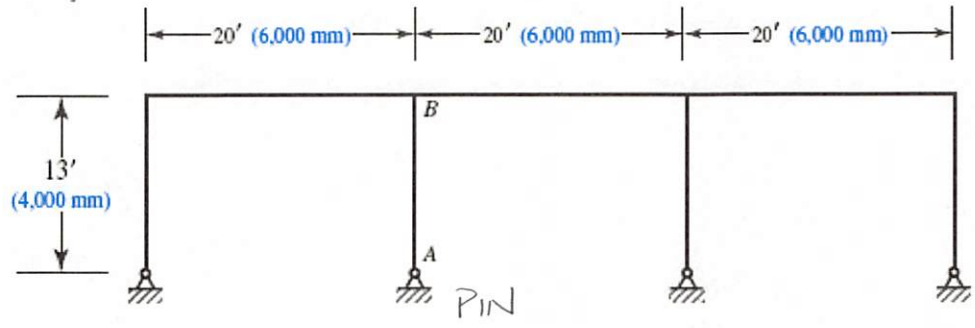


4.7-13 The frame shown in [Figure P4.7-13](#) is unbraced against sidesway. The columns are HSS  $6 \times 6 \times \frac{5}{8}$  (HSS152.4  $\times$  152.4  $\times$  15.9), and the beams are W12  $\times$  22 (W310  $\times$  32.7). ASTM A500 grade B steel ( $F_y = 46$  ksi (315 MPa)) is used for the columns, and  $F_y = 50$  ksi (345 MPa) for the beams. The beams are oriented so that bending is about the  $x$ -axis. Assume that  $K_y = 1.0$ .

- a. Use the alignment chart to determine  $K_x$  for column AB. Use the stiffness reduction factor if applicable. For column AB, the service dead load is 17 kips (76 kN) and the service live load is 50 kips (220 kN).

[SHOW ANSWER](#)

- b. Compute the nominal compressive strength of column AB.



HSS  $6 \times 6 \times \frac{5}{8}$

$$A = 11.7 \text{ in}^2$$

$$I_x = 55.2 \text{ in}^4$$

$$r_x = 2.17 \text{ in}$$

W12  $\times$  22

$$I_x = 156 \text{ in}^4$$

$$I_y = 4.66 \text{ in}^4$$

COLUMN AB

$$G_A = 10^*$$

$$G_B = \frac{55.2/13'}{156 \text{ in}^4/20' + 156 \text{ in}^4/20'} = 0.27$$

FROM ALIGNMENT CHART TABLE C-A-7.2  $K_x \approx 1.7$

$$\frac{L_{c_x}}{r_x} = \frac{1.7(13 \text{ ft})(12 \text{ in/ft})}{2.17 \text{ in}} = 122.21$$

$$4.71 \sqrt{E/F_y} = 4.71 \sqrt{\frac{29,000 \text{ ksi}}{46}} = 118.26$$

4.7-13

$$\frac{L_{cx}}{r_x} > 4.71 \sqrt{E/F_y} \quad \underline{\text{COLUMN IS ELASTIC}} \quad \text{USE E3-3} \quad 2/2$$

$$\frac{L_{cy}}{r} = \frac{K_y L}{r} = \frac{1.0(13\text{ft})(12\text{in/ft})}{2.17\text{in}} = 71.89$$

$$\frac{L_{cx}}{r_x} = 122.21 \quad \text{CONTROLS}^*$$

$$F_e = \frac{\pi^2 E}{(L_{cx}/r)^2} = \frac{\pi^2 (29,000\text{ksi})}{(122.21)^2} = 19.16\text{ksi}$$

$$F_n = 0.877 F_e = 0.877(19.16\text{ksi}) = 16.81\text{ksi}$$

$$P_n = F_n A = 16.81\text{ksi}(11.7\text{in}^2) = \underline{\underline{196.64\text{k}}}$$