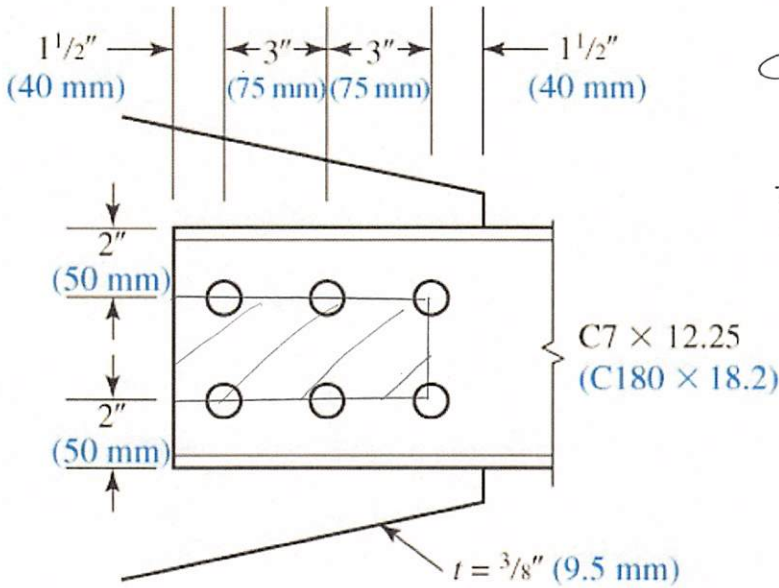


3.5-4 In the connection shown in [Figure P3.5-4](#), ASTM

A572 Grade 50 ($F_y = 50$ ksi (345 MPa); $F_u = 65$ ksi (450 MPa)) steel is used for the tension member, A36 ($F_y = 36$ ksi (250 MPa); $F_u = 58$ ksi (400 MPa)) steel is used for the gusset plate, and the holes are for $3/4$ -inch bolts (M20).



$$d_{\text{hole}} = \frac{3}{4} \text{ in} + \frac{1}{8} \text{ in} = \frac{7}{8} \text{ in}$$

FROM TABLE 1-5 (1-38)

$$t_w = 0.314 \text{ in}$$

$$A_g = 3.59 \text{ in}^2$$

$$\bar{x} = 0.525 \text{ in}$$

$$A_{gv} = 2(0.314 \text{ in})(7.5 \text{ in}) = 4.7100 \text{ in}^2$$

$$A_{nv} = 2(0.314 \text{ in})(7.5 \text{ in} - 2 \cdot \frac{7}{8} \text{ in}) = 3.3363 \text{ in}^2$$

$$A_{nt} = (0.314 \text{ in})(3 \text{ in} - \frac{7}{8} \text{ in}) = 0.6673 \text{ in}^2$$

① IN MEMBER

$$R_n = 0.6 F_u A_{nv} + U_{BS} F_u A_{nt}$$

$$= 0.6(65 \text{ ksi})(3.3363 \text{ in}^2) + (1)(65 \text{ ksi})(0.6673 \text{ in}^2)$$

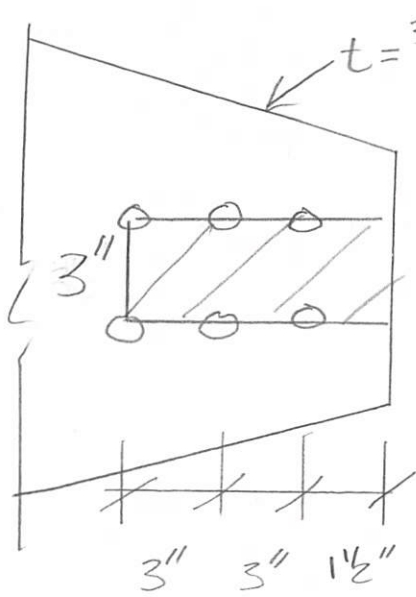
$$= \underline{\underline{1173.49 \text{ k}}}$$

$$\text{UPPER LIMIT} = 0.6 F_y A_{gv} + U_{BS} F_u A_{nt}$$

$$= 0.6(50 \text{ ksi})(4.7100 \text{ in}^2) + (1)(65 \text{ ksi})(0.6673 \text{ in}^2)$$

$$= \underline{\underline{184.67 \text{ k}}}$$

② IN GUSSET PLATE



$$\left. \begin{array}{l} F_y = 36 \text{ ksi} \\ F_u = 58 \text{ ksi} \end{array} \right\} \text{ IN PLATE}$$

$$A_{gv} = \left(\frac{3}{8} \text{ in}\right)(2)(7.5 \text{ in}) = 5.6250 \text{ in}^2$$

$$A_{nv} = \left(\frac{3}{8} \text{ in}\right)(7.5 \text{ in} - 2 \cdot \frac{1}{2}(\frac{7}{8} \text{ in}))(2) = 3.9844 \text{ in}^2$$

$$A_{nt} = \left(\frac{3}{8} \text{ in}\right)(3.0 \text{ in} - 1(\frac{7}{8} \text{ in})) = 0.7969 \text{ in}^2$$

$$P_n = 0.6 F_u A_{nv} + U_{BS} F_u A_{nt}$$

$$= 0.6(58 \text{ ksi})(3.9844 \text{ in}^2) + (1)(58 \text{ ksi})(0.7969 \text{ in}^2)$$

$$= \underline{184.88 \text{ k}}$$

$$\text{UPPER LIMIT } 0.6 F_y A_{gv} + U_{BS} F_u A_{nt}$$

$$= 0.6(36 \text{ ksi})(5.625 \text{ in}^2) + (1)(58 \text{ ksi})(0.7969 \text{ in}^2)$$

$$= \underline{\underline{167.72 \text{ k}}}$$

(3) GROSS SECTION

$$A_g = 3.59 \text{ in}^2$$

$$A_n = A_g - A_{\text{Holes}} = 3.59 \text{ in}^2 - 2(0.314 \text{ in})(\frac{7}{8} \text{ in}) = 3.0405 \text{ in}^2$$

$$A_e = U A_n$$

$$U = 1 - \frac{\bar{x}}{l} = 1 - \frac{0.525 \text{ in}}{6 \text{ in}} = 0.9125$$

$$P_n = F_u A_e = 65 \text{ ksi}(0.9125)(3.0405 \text{ in}^2) = \underline{180.34 \text{ k}}$$

$$P_n = F_y A_g = 50 \text{ ksi}(3.59 \text{ in}^2) = \underline{179.5 \text{ k}}$$

LRFD

$$\text{GROSS TENSION: } 0.9 P_n = 0.9(179.5 \text{ k}) \\ = \underline{161.55 \text{ k}}$$

$$\text{NET TENSION } 0.75 P_n = 0.75(180.34 \text{ k}) \\ = \underline{135.25 \text{ k}}$$

$$\text{BLOCK SHEAR } 0.75 P_n = 0.75(167.72 \text{ k}) \\ = \underline{\underline{125.79 \text{ k} *}}$$

* BLOCK SHEAR GUSSET PLATE CONTROLS *

3.5-4.1

ASD

4/4

GROSS SECTION $\frac{P_n}{1.67} = \frac{179.5^k}{1.67} = \underline{107.49^k}$

NET SECTION $\frac{P_n}{2} = \frac{180.34}{2} = \underline{90.17^k}$

BLOCK SHEAR $\frac{P_n}{2} = \frac{167.72^k}{2} = \underline{\underline{83.86^k}}$

* BLOCK SHEAR IN PLATE CONTROLS *