

Chapter 5.3-4 – Beams

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### Chapter 5 – Stability

- If a beam remains **stable** up to the **fully plastic condition**, the nominal moment strength can be taken as the plastic moment capacity; that is,  $M_n = M_p$
- Otherwise:  $M_n < M_p$
- Instability can be regarded as **overall**, or it can be **local**.
- **Overall buckling** is illustrated below:

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### Chapter 5 – Stability

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### Chapter 5 – Stability

- If a beam remains **stable** up to the **fully plastic condition**, the nominal moment strength can be taken as the plastic moment capacity; that is,  $M_n = M_p$
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- When a beam bends, the **compression** region (above the neutral axis) is analogous to a column, and it will **buckle** if the member is slender enough.

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### Chapter 5 – Stability

- If a beam remains **stable** up to the **fully plastic condition**, the nominal moment strength can be taken as the plastic moment capacity; that is,  $M_n = M_p$
- Otherwise:  $M_n < M_p$
- Unlike a column, the tension portion restrains the compression portion of the cross section, and the outward deflection (**flexural buckling**) is accompanied by twisting (**torsion**).

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### Chapter 5 – Stability

- This form of **instability** is called **lateral-torsional buckling** (LTB).
- Lateral-torsional buckling can be prevented by bracing the beam against twisting at sufficiently close intervals.
- This can be accomplished with **lateral bracing**

**Lateral bracing**, which prevents lateral translation, should be applied as close as possible to the compression flange.

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### Chapter 5 – Stability

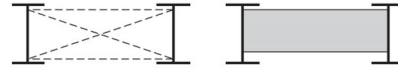
- This form of *instability* is called **lateral-torsional buckling** (LTB).
- Lateral-torsional buckling can be prevented by bracing the beam against twisting at sufficiently close intervals.
- Or this can be accomplished with **torsional bracing**.



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### Chapter 5 – Stability

- This form of *instability* is called **lateral-torsional buckling** (LTB).
- Lateral-torsional buckling can be prevented by bracing the beam against twisting at sufficiently close intervals.
- **Torsional bracing** prevents twist directly; it can be either nodal or continuous, and it can take the form of either cross frames or diaphragms.



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### Chapter 5 – Stability

- This form of *instability* is called **lateral-torsional buckling** (LTB).
- Lateral-torsional buckling can be prevented by bracing the beam against twisting at sufficiently close intervals.
- As we will see, the **moment strength** depends in part on the **unbraced length**, which is the distance between points of bracing.



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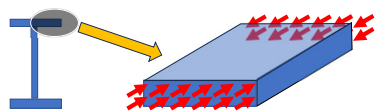
### Chapter 5 – Stability

- Whether the beam can sustain a moment large enough to bring it to the **fully plastic condition** also depends on whether the cross-sectional integrity is maintained.
- This integrity will be lost if one of the **compression elements of the cross-section buckles**.
- This type of buckling can be either compression flange buckling, called **flange local buckling** (FLB), or buckling of the compression part of the web, called **web local buckling** (WLB).
- The type of local buckling that occurs will depend on the **width-to-thickness ratios** of the compression elements of the cross section.

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### Chapter 5 – Stability

- Compression flange buckling, called **flange local buckling**.
- Consider the cross-section below under compression.
- The **flange** is restrained by the web at one edge.

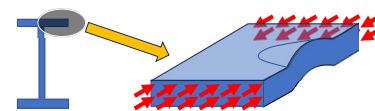


- Failure is localized at areas of high stress (maximum moment) or imperfections.

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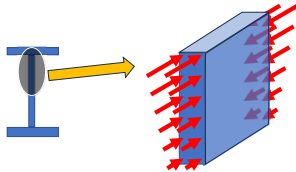


- Failure is localized at areas of high stress (maximum moment) or imperfections.

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### Chapter 5 – Stability

- Compression web buckling is called **web local buckling**.
- Consider the cross-section below under compression.
- The **web** is restrained by the flange at one edge, and the other part of the web is in tension.

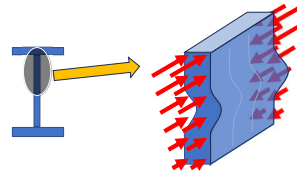


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### Chapter 5 – Stability

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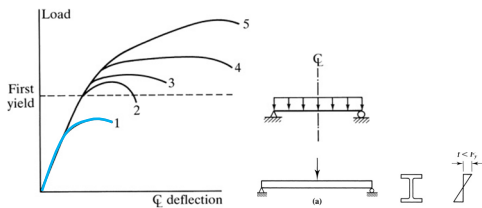


- Failure is localized at areas of high stress (maximum moment) or imperfections.

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### Chapter 5 – Stability

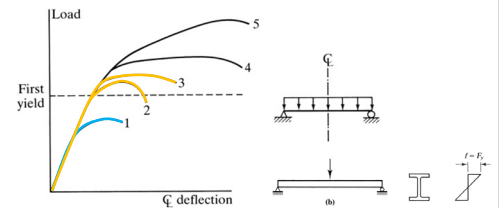
- The graph below shows the effects of **local** and **lateral-torsional buckling**.
- **Curve 1** is the load-deflection curve of a beam that becomes unstable (in any way) and loses its load-carrying capacity before the first yield is attained.



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### Chapter 5 – Stability

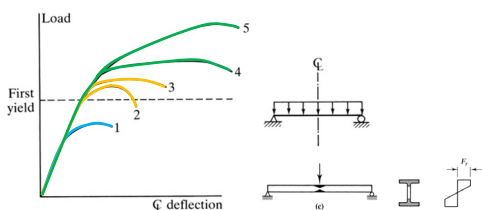
- The graph below shows the effects of **local** and **lateral-torsional buckling**.
- **Curves 2 and 3** correspond to beams that can be loaded past first yield but not far enough for the formation of a plastic hinge and the resulting plastic collapse.



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### Chapter 5 – Stability

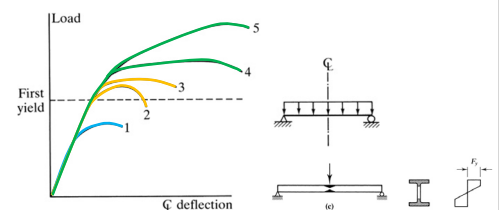
- The graph below shows the effects of **local** and **lateral-torsional buckling**.
- If plastic collapse can be reached, the load-deflection curve will look like either **curve 4** or **curve 5**.



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### Chapter 5 – Stability

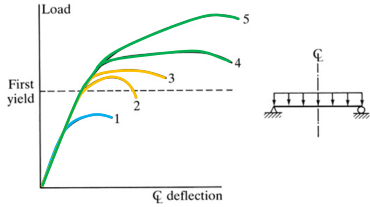
- The graph below shows the effects of **local** and **lateral-torsional buckling**.
- **Curve 4** is for the case of uniform moment over the full length of the beam, and **curve 5** is for a beam with a variable bending moment (moment gradient).



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### Chapter 5 – Stability

- The graph below shows the effects of *local* and *lateral-torsional buckling*.
- *Safe designs* can be achieved with beams corresponding to any of these curves, but *curves 1 and 2* represent *inefficient use of material*.



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### Chapter 5 – Classification of Shapes

- AISC classifies cross-sectional shapes as *compact*, *noncompact*, or *slender*, depending on the values of the *width-to-thickness ratios*.
- *Compact* sections have a slenderness ratio below a certain limit, allowing them to reach their *full yield strength* and form a *plastic hinge without local buckling*.
- *Non-compact* sections have a higher slenderness ratio, meaning some elements will *buckle under a lower stress level* than the full yield strength  $F_y$  before the entire section can become fully plastic.

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### Chapter 5 – Classification of Shapes

- AISC classifies cross-sectional shapes as *compact*, *noncompact*, or *slender*, depending on the values of the *width-to-thickness ratios*.
- For I shapes, the ratio for the projecting flange (an unstiffened element) is  $b_f/2t_f$ , and the ratio for the web (a stiffened element) is  $h/t_w$ .
- The classification of shapes is found in **Section B4** of the Specification, "Member Properties," in **Table B4.1b** (Table B4.1a is for compression members).

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### Chapter 5 – Classification of Shapes

TABLE B4.1b Width-to-Thickness Ratio: Compression Elements Members Subjected to Flexure			
Limit State	Classification of Element	Width-to-Thickness Ratio, $\lambda$	Examples
Local Buckling	(1) Flange of I-shape, channel section, or Z-shape	$\lambda \leq 0.38 \sqrt{E/F_y}$	Compact
	(2) Flange of doubly and singly symmetric I-shape, channel section, or Z-shape	$0.38 \sqrt{E/F_y} < \lambda \leq 0.75 \sqrt{E/F_y}$	Noncompact
	(3) Lip of angle	$\lambda \leq 0.38 \sqrt{E/F_y}$	Compact
	(4) Flange of all I-shape sections and channels in flexure about the minor axis	$0.38 \sqrt{E/F_y} < \lambda \leq 0.75 \sqrt{E/F_y}$	Noncompact
Lateral-Torsional Buckling	(5) Flange of I-shape, channel section, or Z-shape	$\lambda \leq 0.38 \sqrt{E/F_y}$	Compact
	(6) Flange of I-shape, channel section, or Z-shape	$0.38 \sqrt{E/F_y} < \lambda \leq 0.75 \sqrt{E/F_y}$	Noncompact
	(7) Flange of I-shape, channel section, or Z-shape	$\lambda > 0.75 \sqrt{E/F_y}$	Slender
	(8) Flange of I-shape, channel section, or Z-shape	$\lambda > 0.75 \sqrt{E/F_y}$	Slender

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### Chapter 5 – Classification of Shapes

- It can be summarized as follows:
  - $\lambda$  is the *width-to-thickness ratio*,
  - $\lambda_p$  is the upper limit for the *compact* category, and
  - $\lambda_r$  is the upper limit for the *noncompact* category
- Then if  $\lambda \leq \lambda_p$  and the flange is continuously connected to the web, the shape is *compact*;
- if  $\lambda_p < \lambda \leq \lambda_r$  the shape is *noncompact*; and
- if  $\lambda > \lambda_r$  the shape is *slender*.

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### Chapter 5 – Classification of Shapes

- The category is based on the worst *width-to-thickness ratio* of the cross-section.
- For example, if the *web is compact* and the *flange is noncompact*, the shape is classified as *noncompact*.
- From **AISC Table B4.1b** for hot-rolled I-shaped cross-sections.
  - Case 10:  $\lambda = \frac{b_f}{2t_f}$        $\lambda_p = 0.38 \sqrt{\frac{E}{F_y}}$        $\lambda_r = 1.0 \sqrt{\frac{E}{F_y}}$
  - Case 15:  $\lambda = \frac{h}{t_w}$        $\lambda_p = 3.76 \sqrt{\frac{E}{F_y}}$        $\lambda_r = 5.70 \sqrt{\frac{E}{F_y}}$

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**Chapter 5 – Beams**

Any questions?

