

1

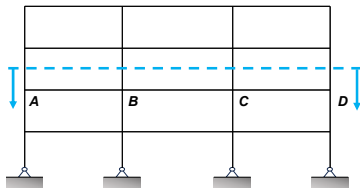
Chapter 5 – Floor and Roof Beams

- When a **distributed load** acts on an area such as a **floor** in a building, certain portions of that load are supported by various components of the floor system.
- The actual distribution is difficult to determine, but it can be approximated quite easily.
- The basic idea is that of **tributary areas**.
- The concept of tributary areas was first discussed in **Section 3.8** in the coverage of **tension members in roof trusses**.

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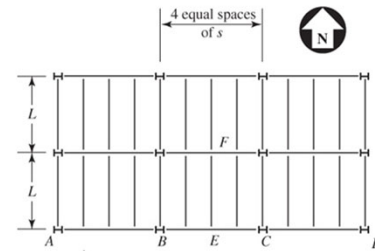
- Consider a typical multistory building.
- Here is one of the rigid frames comprising the building.



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Chapter 5 – Floor and Roof Beams

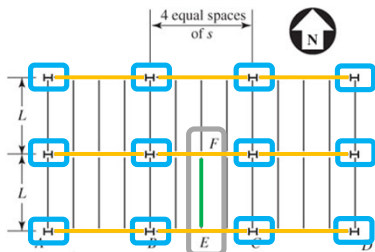
- Here is a **horizontal section** where a cut is made through the building above one of the floors, and the lower portion is viewed from above.



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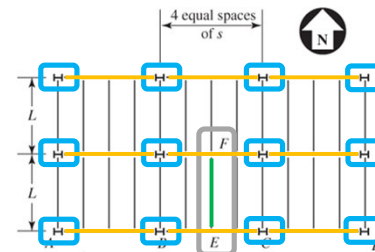
- The gridwork consists of the **column** cross sections, **girders** connecting the columns in the E-W direction, and **floor beams** such as EF spanning between the girders.



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Chapter 5 – Floor and Roof Beams

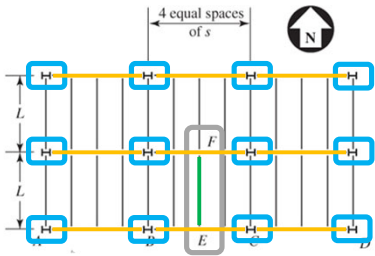
- **Girders** are defined as **beams that support other beams**, although sometimes the term is applied to large beams in general.



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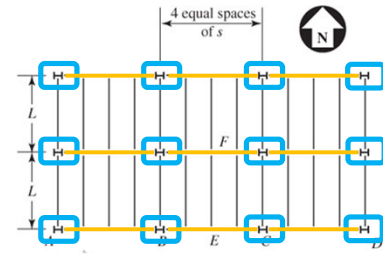
- The **floor beams**, which fill in the panels defined by the columns, are sometimes called **filler beams**.



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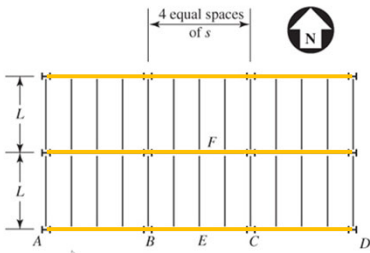
- The **columns** and **girders** along any of the east-west lines make up an **individual frame**.



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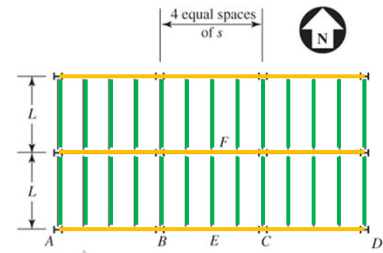
- The **columns** and **girders** along any of the east-west lines make up an **individual frame**.



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Chapter 5 – Floor and Roof Beams

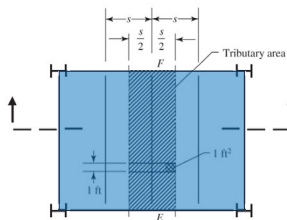
- The **frames** are connected by the **beams in the north-south** direction, completing the framework for the building.



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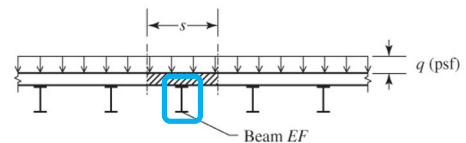
- Consider a typical bay of the floor framing system.
- When columns are placed in a rectangular grid, the region between four columns is called a **bay**.



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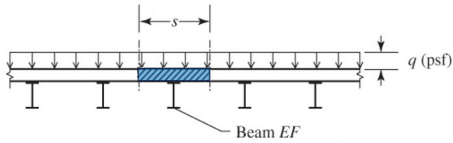
- Here is a cross-section of this bay, showing the **floor beams** as wide-flange steel shapes.



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Chapter 5 – Floor and Roof Beams

- Here is a cross-section of this bay, showing the **floor beams** as wide-flange steel shapes.
- Supporting reinforced concrete floor slabs.



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Chapter 5 – Floor and Roof Beams

- One of the objectives of a structure is to **transmit loads to the foundation**.
- For floor loads, this transmission of loads is accomplished as follows:
 1. Floor loads, both **live and dead**, are supported by the **floor slab**.
 2. The weight of the slab, along with the loads it supports, is supported by the **floor beams**.
 3. The floor beams transmit their loads, including their own weight, to the **girders**.

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Chapter 5 – Floor and Roof Beams

- One of the objectives of a structure is to **transmit loads to the foundation**.
- For floor loads, this transmission of loads is accomplished as follows:
 4. The girders and their loads are supported by the **columns**.
 5. The column loads are supported by the **columns of the story below**.

The column loads accumulate from the top story to the **foundation**.

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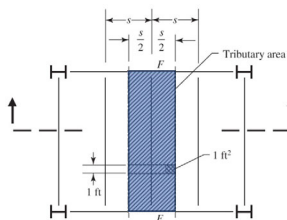
Chapter 5 – Floor and Roof Beams

- The **route taken by the loads** from one part of the structure to another is sometimes called the **load path**.
- This is a fairly accurate representation of what happens, but it is not exact.
- For example, part of the **slab** and its load will be supported directly by the **girders**, but most of it will be carried by the **floor beams**.

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Chapter 5 – Floor and Roof Beams

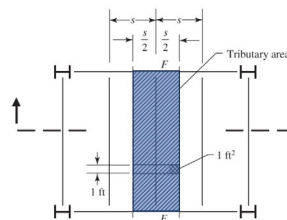
- The **tributary area** for beam EF is the **shaded area**.
- It consists of **half the floor** between beam EF and the adjacent beam on each side.



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Chapter 5 – Floor and Roof Beams

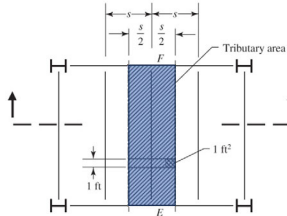
- Thus, the total width of the floor being supported is equal to the **beam spacing, s**, if the spacing is uniform.
- If the load on the floor is uniformly distributed, we can express the uniform load on beam EF as a **force per unit length**.



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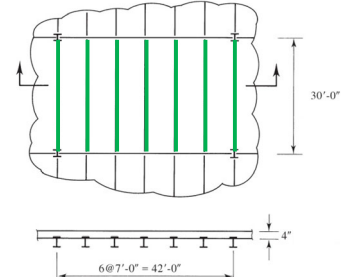
- The weight of a **reinforced concrete floor slab** is usually expressed in pounds per square foot (*psf*) of floor surface.
- This way, the **slab weight** can be combined with other loads similarly expressed.



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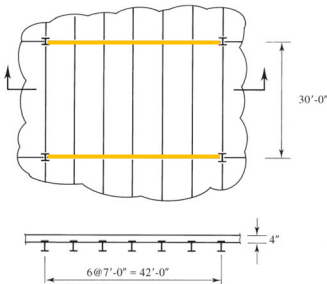
- **Example 5.15:** Consider a floor framing system with a 4-in thick reinforced concrete floor slab of normal-weight concrete is supported by floor beams spaced at 7 ft.



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Chapter 5 – Floor and Roof Beams

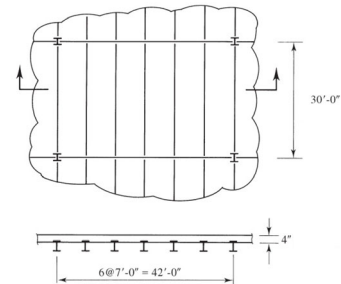
- **Example 5.15:** The floor beams are supported by girders, which in turn are supported by the columns.



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Chapter 5 – Floor and Roof Beams

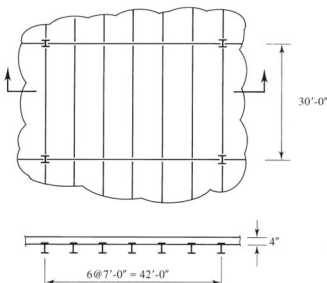
- **Example 5.15:** Loads include a uniform live load of 80 *psf* and moveable partitions, which are accounted for using a uniformly distributed load of 20 *psf* on the floor surface.



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Chapter 5 – Floor and Roof Beams

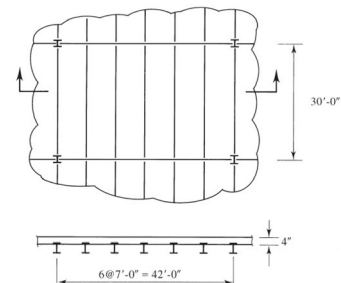
- **Example 5.15:** The maximum live load deflection must not exceed $L/360$.



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Chapter 5 – Floor and Roof Beams

- **Example 5.15:** Use **A992** steel $F_y = 50$ *ksi* and design the floor beams. Assume that the slab provides continuous lateral support for the floor beams.



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Chapter 5 – Floor and Roof Beams

➤ **Example 5.15:** The slab weight is:

$$w_{slab} = \frac{t}{12in/ft} (150psf) = \frac{4in}{12in/ft} (150psf) = 50psf$$

Each beam supports a 7-ft width (tributary width) of floor.

Slab: = 50psf (7 ft) = 350lb/ft

Partitions: = 20psf (7 ft) = 140lb/ft

Live load: = 80psf (7 ft) = 560lb/ft

The **beam weight** will be accounted for once a trial selection has been made.

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Chapter 5 – Floor and Roof Beams

➤ **Example 5.15:** Since the partitions are movable, they will be treated as live load. The dead and live loads are:

$$w_D = 0.350k/ft$$

$$w_L = 0.560k/ft + 0.140k/ft = 0.7k/ft$$

LRFD solution:

$$w_u = 1.2(0.35k/ft) + 1.6(0.7k/ft) = 1.54k/ft$$

The typical floor beam connection provides virtually no moment restraint, so the beams can be treated as **simply supported**.

$$M_u = \frac{w_u L^2}{8} = \frac{(1.54k/ft)(30ft)^2}{8} = 173kft$$

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Chapter 5 – Floor and Roof Beams

➤ **Example 5.15:** The maximum permissible live-load deflection is:

$$\Delta_L = \frac{5w_L L^4}{384EI} \quad \Delta_L = \frac{L}{360} = \frac{360in}{360} = 1.0in$$

$$\Rightarrow I_{required} = \frac{5w_L L^4}{384E\Delta_L} = \frac{5(0.7k/ft)(1ft/12in)(360in)^4}{384(29,000ksi)(1.0in)} = 440in^4$$

Since the beams have continuous lateral support, the I_x table can be used to select a trial shape that will satisfy the moment requirement.

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Chapter 5 – Floor and Roof Beams

➤ **Example 5.15:**

From Table 3-3 (3-29):

W18 x 35

$$I_x = 510in^4 > I_{required}$$

O.K.

Shape	I_x	Shape	I_x	Shape	I_x	Shape	I_x
W10-30	303	W16-42	1030	W18-48	612	W12-22	139

Shape	I_x	Shape	I_x	Shape	I_x	Shape	I_x
W20-90	3610	W26-62	1550	W18-40	612	W12-22	139
W12-200 ¹	3550	W18-88	1530	W12-72	597	W8-40	146
W24-117	3540	W14-132	1530	W16-45	586	W10-26	144
W18-175	3460	W16-100	1480	W14-53	541	W12-19	130
W14-257	3400	W21-68	1480	W18-88	534	W8-35	127
W27-94	3270	W12-152	1430	W12-65	533	W10-22	118
W21-132	3220	W14-120	1380	W12-50	510	W8-31	110
W12-279 ¹	3110	W26-55	1350	W18-35	510	W12-16	103
W24-104	3100	W21-62	1330	W16-30	475	W8-28	98.0
W16-156	3060	W18-76	1330	W12-58	475	W10-19	96.3
W14-233	3010	W16-89	1300	W10-77	455	W8-24	82.7
W24-102	3000	W14-109	1240	W18-36	448	W12-14	86.6
W21-122	2960	W12-136	1240	W14-53	428	W10-17	81.9
W27-84	2890	W21-57	1170	W14-43	428	W8-21	75.3
W18-143	2750	W18-71	1170	W10-69	394	W10-15	68.9
W12-252 ¹	2720	W21-55	1140	W12-50	381	W8-18	61.9
W24-94	2700	W18-77	1110	W14-36	385	W10-12	58.8

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Chapter 5 – Floor and Roof Beams

➤ **Example 5.15:**
From Table 3-2 (3-26):

$$\phi_b M_n = 249kft > M_u = 177kft$$

O.K.

$$V_u = \frac{w_u L}{2} = \frac{(1.54k/ft)(30ft)}{2} = 23.1k$$

$$\phi_v V_n = 159k > V_u$$

O.K.

Shape	Z_x	M_n	$\phi_b M_n$	M_u	$\phi_b M_u$	M_n	$\phi_b M_n$	M_u	$\phi_b M_u$	L_p	L_r	I_x	V_n	$\phi_v V_n$
W18-35	66.5	160	249	101	151	8.14	12.3	4.31	12.3	510	106	139	159	159
W16-36	64.0	160	240	98.7	148	8.24	9.36	5.37	15.2	448	93.6	141	151	151
W14-38	61.5	153	231	95.4	143	5.37	8.20	5.47	16.2	385	87.4	131	131	131
W10-49	60.4	151	227	95.4	143	2.46	3.71	8.97	31.6	272	68.0	102	102	102
W8-58	59.8	149	224	90.8	137	1.70	2.55	7.42	41.6	228	99.3	134	134	134
W12-40	57.0	142	214	89.9	135	3.66	5.54	8.85	21.1	307	70.2	105	105	105
W10-45	54.9	137	206	85.3	129	2.59	3.89	7.10	26.9	248	70.3	106	106	106
W14-34	54.6	136	205	84.9	128	5.01	7.85	5.40	15.6	349	79.8	120	120	120
W18-21	54.0	135	203	82.4	124	6.86	10.3	4.13	11.8	375	87.8	131	131	131
W12-35	51.2	128	192	79.6	120	4.34	6.45	5.44	16.6	285	75.0	113	113	113
W8-48	49.0	122	184	75.4	113	1.07	2.55	7.35	35.2	184	68.0	102	102	102

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Chapter 5 – Beam Design Charts

➤ **Example 5.15:** In this example, the design was controlled by **serviceability** rather than **strength**.

This is not unusual.

Although there is **no limit on the dead load** deflection in this example, this deflection may be needed if the beam is to be **cambered**.

$$\Delta_D = \frac{5(w_{slab} + w_{beam})L^4}{384EI} = \frac{5(0.35k/ft + 0.035k/ft)(1ft/12in)(360in)^4}{384(29,000ksi)(510in^4)} = 0.474in$$

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Chapter 5 – Beam Design Charts

Let's work on some problems



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Chapter 5 – Beams

Any questions?



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